

Development and evaluation of virtual refrigerant mass flow sensors for fault detection and diagnostics



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ABSTRACT

Refrigerant mass flow rate is an important measurement for monitoring equipment performance and enabling fault detection and diagnostics. This paper presents and evaluates three different virtual refrigerant mass flow (VRMF) sensors that use mathematical models to estimate flow rate using low cost measurements. The first model uses a compressor map that relates refrigerant flow rate to measurements of condensing and evaporating saturation temperature, and to compressor inlet temperature measurements. The second model uses an energy-balance method on the compressor that uses the compressor power consumption. The third model is developed using an empirical correlation for an electronic expansion valve (EEV) based on an orifice equation. The three VRMFs are shown to work well in estimating refrigerant mass flow rate for various systems under fault-free conditions with less than 5% RMS error. The combination of the three VRMFs can be utilized to detect and diagnose when the compressor and/or expansion device is not providing the expected flow.

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Développement et évaluation de capteurs virtuels de débit massique de frigorigène pour la détection de défaut et les diagnostics

Mots clés : Capteur virtuel ; Débit massique de frigorigène ; Détection de défaut et diagnostic ; Compresseur ; Dispositif de détente ; Contrôle de performance

1. Introduction

Space heating, ventilation and air conditioning (HVAC) account for 40% of residential primary energy use, and for 30% of primary energy use in commercial buildings (Energy Efficiency and Renewable Energy, 2008). Over half of all conditioned floor space in the U.S. incorporates packaged HVAC equipment in their system design (Brodrick, 2000). The study conducted by Messenger (2008) indicates unitary air conditioners typically

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Nomenclatur	e
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А	area [m²]	V	volume flow rate $[m^3 s^{-1}]$
C	empirical coefficient for expansion valve	VRMF	virtual refrigerant mass flow sensor
a, b, c	empirical constants	X ₀	threshold partitioned into two regions, R_1 and R_2
$C_{d,eev}$	correction coefficient for EEV model	Y	vector of current residuals
D	diameter		
d	current needle diameter [m]	Subscripts	
EER	energy efficiency ratio	actual	actual
EEV	electronic expansion valve	b	bulb
EEVSTEP	opening of EEV [step]	С	current
E(x)	expected value of x	С	condenser
F	force [N]	cri	critical
f	compressor speed [Hz]	current	current
FDD	fault detection and diagnostics	diaph	diaphragm
Н	maximum needle position [m]	dis	discharge
h	certain needle position [m]	е	evaporator
h	enthalpy [kJ kg ⁻¹]	f	liquid
h(x)	discriminant function	g	gas
K _{flow}	ratio of refrigerant volumetric flow rate at	max	maximum
,	operating speed to value at rated speed	measured	measurement
kon	spring constant [N m ⁻¹]	min	minimum
l(x)	likelihood ratio	Ν	normal
MN	mean vector matrix without fault	orifice	orifice
Mc	mean vector matrix with fault	pin	needle
M	mean vector matrix describing the distribution	pred	estimation
	of residuals	rated	rated condition
\dot{m}_{map}	refrigerant mass flow rate based on compressor	sat	saturation
	map [kg s ⁻¹]	sp	spring
\dot{m}_{energy}	refrigerant mass flow rate based on compressor	sp,cl	closed spring
	energy balance [kg s ⁻¹]	suc	suction
\dot{m}_{TXV}	refrigerant mass flow rate based on TXV model	TXV	thermostatic expansion valve
$\dot{m}_{\rm EEV}$	refrigerant mass flow rate based on EEV model	Greek	
	[kg s ⁻¹]	ρ	density [kg m ⁻³]
Р	pressure [Pa]	<i>α</i> loss	compressor heat loss ratio
P(x)	mixture density function	δ	spring deflection [m]
$P(w_i/x)$	conditional probability of ω_i given that x	μ_{i}	mean of residual
$P(w_i)$	prior density function	Σ_1	covariance matrix without fault conditions
R	region	Σ_2	covariance matrix with fault conditions
S	weighted average	2	Bayesian classification error
SC	subcooling [K]	n	Mahalanobis distance
TXV	thermostatic expansion valve	σ	standard deviations
Т	temperature [K]	0 0	class i
t	frequency parameter of the Fourier transform	V-	threshold for given distribution
117	compressor input nower [W]	ξ.	standard normal random variable
V	optimum coefficient	5	
	optimum coemercit		

do not achieve rated efficiency because of improper installation or lack of servicing in the field. This paper suggested that service and replacement programs can yield energy savings on the order of 30–50%. The other study from ADM (2009) evaluated 109 units in the field and found that 89 had fault conditions, with 31 having two or more faults. The average energy efficient ratio (EER) for the units increased from 6.6 before servicing to 7.0 after servicing, an average increase of 6.1%. Another investigation (Katipamula and Brambley, 2005) suggested that faults or non-optimal control can cause the malfunction of equipment or performance degradation from 15 to 50%. Automated diagnostics has the potential to address these field performance problems and produce significant energy savings.

Even though various fault detection and diagnostic (FDD) studies (Kim et al., 2009; Li and Braun, 2007; Rossi and Braun, 1997) have been carried out for air conditioner and heat pump systems with fixed speed compressors and fixed orifice expansion (FXO) valves, FDD research for systems with variable speed compressors and electronic expansion valves (EEV) has been limited. The use of variable speed compressors is common

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