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# A theoretical study on a novel solar based integrated system for simultaneous production of cooling and heating

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## ABSTRACT

An integrated system for simultaneous production of triple-effect cooling and single stage heating is proposed in this paper to harness low grade solar energy. The proposed system combines the heliostat field with a central receiver and the ejector-absorption cycle with the shaft power driven transcritical CO<sub>2</sub> cycle. A parametric study based on first and second laws of thermodynamics is carried out to ascertain the effect of varying the exit temperature of duratherm oil, turbine inlet pressure, and evaporators temperature on the energy and exergy output as well as on the energy and exergy efficiencies of the system. The results obtained indicate that major source of exergy destruction is the central receiver where 52.5% of the inlet solar heat exergy is lost followed by the heliostat where 25% of the inlet exergy is destroyed. The energy and exergy efficiencies of the integrated system vary from 32% to 39% and 2.5%–4.0%, respectively, with a rise in the hot oil outlet temperature from 160 °C–180 °C. It is further shown that increase in evaporator temperature of transcritical CO<sub>2</sub> cycle from –20 °C to 0 °C increases the energy efficiency from 27.45% to 43.27% and exergy efficiency from 2.51% to 2.97%, respectively. The results clearly show how the variation in the values of hot oil outlet temperature, turbine inlet pressure, and the evaporator temperature of transcritical CO<sub>2</sub> cycle strongly influences the attainable performance of the integrated system.

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# Une étude théorique sur un nouveau système intégré à base d'énergie solaire pour la production simultanée de refroidissement et de chauffage

Mots clés : A base solaire ; Système intégré ; Refroidissement ; Chauffage ; Exergie

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Nomenclature			
$A_{ap}$	aperture area [m <sup>2</sup> ]	A	absorber
$A_{field}$	area of heliostat field [m <sup>2</sup> ]	$A_p$	aperture
ARC	absorption refrigeration cycle	C1, C2, C3	condensers
Comp	compressor	comp	compressor
C	concentration ratio	CR	central receiver
C2	condenser of the absorption refrigeration cycle	D	destruction
COP	coefficient of performance	d	diffuser
CO <sub>2</sub>	carbon dioxide	E1, E2, E3	evaporators
$\Delta \dot{E}$	exergy change [kJ s <sup>-1</sup> ]	EJE	ejector
EJE	ejector	f	refrigerant fluid
E3	evaporator of the transcritical CO <sub>2</sub> cycle	GC	gas cooler
$\dot{E}$	exergy rate [kJ s <sup>-1</sup> ]	GEN	generator
E	evaporator	H	heating
ERC	ejector refrigeration cycle	HRVG	heat recovery vapor generator
GEN	generator	is	isentropic process across the turbine/compressor
h	specific enthalpy [kJ kg <sup>-1</sup> ]	IHX	internal heat exchanger
LiBr–H <sub>2</sub> O	lithium bromide–water	mf	mixed stream flow
$\dot{m}$	mass flow rate [kg s <sup>-1</sup> ]	m	mixing chamber
ORC	organic Rankine cycle	n1	inlet of nozzle
P	pressure [Pa]	n2	outlet of nozzle
$\dot{Q}$	energy rate [kJ s <sup>-1</sup> ]	n	nozzle
q	solar radiations received per unit area or DNI [Wm <sup>-2</sup> ]	oil	hot oil (Duratherm600)
R-123	2,2-Dichloro-1,1,1-trifluoroethane	P	pump
s	specific entropy [kJ kg <sup>-1</sup> K <sup>-1</sup> ]	pf	primary flow
TC	transcritical CO <sub>2</sub> cycle	r	water refrigerant
T	absolute temperature [K]	sf	secondary flow
U	velocity [ms <sup>-1</sup> ]	SHX	solution heat exchanger
$\dot{W}$	rate of work done [kJ s <sup>-1</sup> ]	s	solution mixture of LiBr–H <sub>2</sub> O
Greek symbols		s'	state at the end of isentropic process across the nozzle/diffuser of the ejector
$\mu$	entrainment ratio	th	thermal
$\eta$	efficiency [%]	T	turbine
Subscript		TV	throttling valve
		1, 2, 3,.....a, b, c	state points in Fig. 1

## 1. Introduction

During the last few decades, an increasing interest, based on research and development, has been concentrated on utilization of solar energy more aggressively to address the world energy and environmental situation. The possibility of utilizing solar energy for the production of cooling and heating has attracted Man's attention since the early development of solar technology (Grossman (2002), Petela (2009)). Solar powered cooling is regarded as a promising technology due to the close coincidence of very high air-conditioning and refrigeration demands in peak summers when there is maximum available solar energy. This offers an excellent opportunity to meet out the increasing energy demand for cooling of various countries of the gulf region where more than 60% of the power produced is used for refrigeration and air-conditioning purposes (Ratlamwala et al. (2013)). Recently, rapid development occurred worldwide in the basic technology and market strategy for the concentrating solar power (CSP) technologies,

including parabolic trough, power tower, and dish/engine (Yao et al. (2009), Larbi et al. (2010), Montes et al. (2011)).

The superiority of second law analysis over the traditional first law methods for energy conversion processes in general and solar thermal technology in particular has been widely recognized due to the fact that latter does not distinguishes the quantity and quality of energy and simply provides the overall performance of the system. On the other hand, combined first and second law analysis which is called the exergy analysis gives a clearer assessment of various losses occurring in energy systems both quantitatively and qualitatively and the irreversibilities in the system and thereby shows the possibilities where improvements in efficiency could be made (Bejan (2002), Dincer and Rosen (2007), Hepbasli (2008)).

In this context, throughout the literature, there are numerous studies reporting the second law performance of solar driven absorption refrigeration cycle, ejector refrigeration cycle, and combined ejector-absorption refrigeration cycle. Chua et al. (2002) modeled and developed an irreversible

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