

Feasibility study of a bowtie compressor with novel capacity modulation

Jun-Hyeung Kim*, Eckhard A. Groll

School of Mechanical Engineering, Ray W. Herrick Laboratories, Purdue University, West Lafayette, IN 47907, USA

Received 14 November 2006; received in revised form 27 February 2007; accepted 21 March 2007

Available online 28 March 2007

Abstract

A novel refrigeration compressor with an integrated method of capacity modulation for use in domestic refrigerators/freezers is proposed and analyzed here. The compressor is called bowtie compressor due to its two sector-shaped, opposing compression chambers forming a bowtie. The bowtie compressor modulates the cooling capacity by changing the piston stroke without changes of the clearance volume for better thermodynamic efficiency. The new compressor includes a unique off-center-line mechanism so that the piston stroke can be varied without creating an extra clearance volume. To investigate the feasibility of the proposed compressor, a simulation model has been developed. A detailed description of the bowtie compressor and its simulation model are presented in this paper. In addition, parametric studies have been carried out to see how the proposed compressor performance can be improved.

© 2007 Elsevier Ltd and IIR. All rights reserved.

Keywords: Domestic refrigerator; Design; Compressor; Oscillating compressor; Capacity reduction; Simulation; Performance

Compresseur « nœud de papillon » muni d'un nouveau dispositif de modulation : Étude de faisabilité

Mots clés : Réfrigérateur domestique ; Conception ; Compresseur ; Compresseur oscillant ; Réduction de puissance ; Simulation ; Performance

1. Introduction

The compressor of typical domestic refrigerators/freezers is designed to deliver the full cooling capacity at

a single speed. Since the cooling capacity of domestic refrigerators/freezers varies throughout their operation, the capacity of the compressor has to be modulated to match the cooling loads. Conventional compressors are designed to operate at the maximum cooling load. As a result, they cycle on and off in response to the change of the cooling load. This on-and-off operation is not efficient and consumes unnecessary amounts of energy whenever the compressors are turned back on. One way to increase the efficiency of the compressors is to continuously modulate the compressor capacity based on the demand of the cooling load.

* Corresponding author. Tel.: +1 765 496 5143; fax: +1 765 496 0787.

E-mail addresses: phiengineer@gmail.com (J.-H. Kim), groll@purdue.edu (E.A. Groll).

Nomenclature

A	area (m^2)	θ_{01}	angle of the eccentricity vector (radian)
$A(t)$	time-dependent heat transfer area (m^2)	θ_{02}	angle of the ground vector (radian)
BDC	bottom-dead-center	θ_{12}	angle of the connecting rod vector (radian)
C_D	drag coefficient		
C_v	specific heat at constant volume ($\text{J kg}^{-1} \text{K}^{-1}$)	<i>Superscript</i>	
D	diameter (m)	\rightarrow	vector
h	enthalpy (J kg^{-1})	$-$	average
$h(t)$	heat transfer coefficient ($\text{W m}^{-2} \text{K}^{-1}$)	<i>Subscripts</i>	
k_s	spring stiffness (N m^{-1})	amb	ambient
$K(t)$	thermal conductivity of the gas ($\text{W m}^{-1} \text{K}^{-1}$)	cir	circumference of the valve
l	initial length between the centers of the crank and the journal shafts (m)	comp	compression
m	refrigerant mass (kg)	cond	condensing
m_{eq}	equivalent mass of the plate spring (kg)	cv	clearance volume
\dot{m}	mass flow rate (kg s^{-1})	cyl	cylinder
P	pressure (Pa)	dis	discharge
\dot{Q}	heat transfer rate (W)	evap	evaporating
r_{01}	length of the eccentricity (m)	f	flux force
r_{02}	length of the ground vector (m)	flow	effective flow of the port
r_{24}	length of the journal shaft vector (m)	friction	friction
r_{25}	length of the vane vector (m)	gas	gas
R	thermal resistance (K W^{-1})	high	high-side
\vec{R}_{01}	eccentricity vector	in	into the cylinder
\vec{R}_{13}	connecting rod vector	leak	leakage
\vec{R}_{25}	vane vector	loss	loss
rpm	rotation per minute	low	low-side
t	time (s)	m	mechanical
T	temperature (K)	motor	motor
TDC	top-dead-center	o	total
U_{piston}	mean piston speed (m s^{-1})	oil	oil
V	velocity (m s^{-1})	o,s,c	overall isentropic compressor
\forall	volume (m^3)	out	out of the cylinder
x	x directional coordinate or x distance or control length (cm)	p	pressure force
		piston	piston
<i>Greek letters</i>		port	port
γ	specific heat ratio	rad	radiation
η	efficiency	shell	in the shell
$\mu(t)$	dynamic viscosity of the gas (Pa s)	suct	suction
v	specific volume ($\text{m}^3 \text{kg}^{-1}$)	super	superheating
ω	angular velocity (s^{-1})	swept	swept
ω_{12}	angular velocity of the journal shaft (s^{-1})	th	throat of a valve port
$\omega_{n,1}$	natural frequency at the first mode shape (s^{-1})	tr	transitional
ρ	density (kg m^{-3})	v	volumetric
θ	angle (radian)	valve	valve
		wall	cylinder wall

A typical method for continuous capacity modulation is variable speed control in which a variable speed motor controls the speed of the piston stroke to match the cooling loads. Theoretical studies by Holdcack-Janssen and Kruse [1], and Zubair and Bahel [2] reported that variable speed control is the most energy efficient capacity control method at full and part load conditions in comparison to on/off

control, hot gas bypass, clearance volume control, and cylinder unloading. In addition, variable speed control introduces the following other advantages: (1) precise thermal control is possible; (2) the reliability of the compressor is improved due to the reduced number of on/off cycles; (3) the response time for set conditions is fast. However, variable speed control is the most expensive method among the other capacity

Download English Version:

<https://daneshyari.com/en/article/792944>

Download Persian Version:

<https://daneshyari.com/article/792944>

[Daneshyari.com](https://daneshyari.com)