



# Development of a dynamic model for natural ventilated photovoltaic components and of a data driven approach to validate and identify the model parameters

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## Abstract

In the development of dynamic models for the energy performance evaluation of building integrated natural ventilated PV components there are still many open questions regarding the uncertainty of the estimated parameters of the models. Traditionally, the dynamic models for these complex components are derived from the heat transfer balance equations, and the unknown heat transfer coefficients (convection and radiation), the solar properties of the materials or the pressure coefficients for the air mass flow rate balance, are assigned based on literature or on manufacturer prescriptions. However, there is a lack of systematic methods able to validate the simulation outputs with the measured data, taking into consideration the uncertainty of the parameters and their effect over the results. This research is focused on the development of a dynamic simulation model for a PV ventilated component, and on the application of a data-driven iterative approach to identify the unknown parameters, to evaluate their influence in the simulation outputs and finally, to determine the deviations of the simulations outputs against the measured data. During the identification process, 43 unknown parameters are detected and 13 of them are categorized as strong parameters. The implemented data driven approach is able to achieve high goodness of fit with the measured data and it is recommended to analyses which aim at evaluating the influence of some component parameters or the thermal and electrical energy produced by these natural ventilated PV components.

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**Keywords:** Building integrated photovoltaics; Dynamic simulation modeling; Data driven optimization; Sensitivity analysis; Latin Hypercube Monte Carlo

## 1. Introduction

For the last years, many authors have been working in the field of double skin ventilated photovoltaic (PV) components with and without building integrated photovoltaics (BIPV). Since the 1990's Hans Bloem,

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**Nomenclature**

$A$	area (m <sup>2</sup> )	$\tau$	solar transmittance (–)
$b$	depth of the air gap (m)	$\rho$	density (kg/m <sup>3</sup> )
$C_d$	discharge coefficient (–)	$\nu$	kinematic viscosity (m <sup>2</sup> /s)
$c_p$	specific heat capacity of the air (J/kg °C)	$\mu$	dynamic viscosity (kg/m s)
$d$	length of the finite elements (m)	$\eta$	unitary vector at normal direction (–)
$D_h$	hydraulic diameter (m)	$\eta_{PV}$	photovoltaic cells efficiency at standard conditions (–)
$g$	gravitational acceleration (m/s <sup>2</sup> )	$\theta$	incident angle (°)
$G$	incident solar radiation (W/m <sup>2</sup> )		
$B$	buoyancy term, (–), $B = 2SGr_{D_h}/Pr$		
$\bar{h}$	average convective heat transfer coefficient (W/m <sup>2</sup> °C), $\bar{h} = \bar{Nu} \cdot k/D_h$	<i>Subscripts</i>	
$h_r$	linearized radiative heat transfer coefficient (W/m <sup>2</sup> °C)	$a$	ambient
$h_i$	thickness of each solid layer (m)	$app$	apparent
$H$	height of the ventilated PV component (m)	$b$	beam
$H^+$	dimensionless height, (–), $H^+ = H/2bRe$	$c$	front node of the PV laminate
$k$	thermal conductivity (W/m °C)	$cond$	conduction
$k_h$	inlet and outlet hydraulic losses (–)	$d$	diffuse
$\dot{m}$	air mass flow rate (kg/s)	$e$	back node of the PV laminate
$\bar{Nu}$	average Nusselt number (–)	$e_i$	thickness of the solid layers
$P$	Packing factor (–), $P = A_{PV}/A_T$	$f$	air or fluid
$Pr$	Prandtl number (–)	$g$	rear facing material
$q''$	specific heat flux (W/m <sup>2</sup> )	$g1$	front node of the rear facing material
$q''_e$	specific electrical production of the PV laminate (W/m <sup>2</sup> )	$g2$	back node of the rear facing material
$Q$	volumetric heat source (W/m <sup>3</sup> )	$gPV$	clear glass of the PV module
$Ra''_b$	modified Rayleigh number for uniform heat flux boundary conditions, (–), $Ra'' = \rho^2 g \beta c_p q''_w b^5 / \mu k^2 H$	$h$	horizontal
$Re$	Reynolds number (–)	$i$	inlet
$S$	coefficient of stratification (–)	$m$	weather station
$S_g$	solar radiation absorbed by the solid layers (W/m <sup>2</sup> )	$n$	normal
$T$	average temperature of the air gap at a fixed height (°C)	$o$	outlet
$y$	vertical distance (m)	$PV$	photovoltaic cells
$W$	width of the ventilated PV component (m)	$PV1$	node of the PV cells layer
		$r$	radiation
		$s$	sky
		$t$	turbulent
		$tr$	semi transparent surface
		$T$	total surface
		$wc$	cold wall
		$wh$	hot wall
<i>Greek letters</i>		<i>Superscripts</i>	
$\alpha$	solar absorptivity (–)	$b$	back
$\varepsilon$	total hemispherical emissivity (–)	$f$	front
$\sigma$	Stefan Boltzman constant, $\sigma = 5.67 \cdot 10^{-8}$ (–)		

Bloem et al. (2004), Bloem and van Dijk (2000), Bloem et al. (1997) and Bloem (2008) have been carrying out an intensive characterization of PV ventilated components, with and without ventilated air gaps. Some European funded projects have been actively supporting this work, PASSLINK, PV-HYBRIDPAS and IMPACT (Strachan and Vandaele, 2008). Between 1999 and 2000, Mei et al. (2003) undertook the theoretical analysis and monitoring of the Mataro's public library building, which had the first PV ventilated façade in Europe. More recently, the

treatment of the induced flow and the heat transfer at the air gap and the surfaces of a natural ventilated double skin façade has been progressively refined by Brinkworth (2000a), Brinkworth et al. (2000), Brinkworth (2000b) and Brinkworth and Sandberg (2006). Concerning to the mathematical model to define the energy performance of such PV components, simplified methods have been proposed by Ursula Eicker (2003) and Mei et al. (2003). More sophisticated models for double skin façades have been also developed by Faggembaau et al. (2003) and Saelens

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