



Available online at www.sciencedirect.com

ScienceDirect



Solar Energy 103 (2014) 200-209

www.elsevier.com/locate/solener

Smart windows: Thermal modelling and evaluation

M. Sabry^{a,b,*}, P.C. Eames^c, H. Singh^d, Yupeng Wu^e

^a Physics Dept., College of Applied Science, Umm Al Qura University, Makkah, Saudi Arabia
 ^b National Research Institute of Astronomy and Geophysics, Cairo, Egypt
 ^c CREST, Loughborough University, Loughborough LE11 3TU, UK
 ^d School of Engineering and Design, Brunel University, Uxbridge UB8 3PH, UK

^e School of Engineering, Nottingham University, UK

School of Engineering, Nottingham University, UK

Received 20 July 2013; received in revised form 31 January 2014; accepted 6 February 2014 Available online 4 March 2014

Communicated by: Associate Editor G.N. Tiwari

Abstract

A numerical investigation of the performance of a multi paned smart window integrated with water-cooled high efficiency third generation GaAsP/InGaAs QWSC (\sim 32% efficiency) solar cells illuminated by two-axis tracking solar concentrators at 500× in the inter pane space is presented. Optimising system parameters such as optical concentration ratio and coolant (water) flow rate is essential in order to avoid degradation in system performance due to high cell temperatures and thermal stresses. Detailed modelling of the thermo-fluid characteristics of the smart windows system was undertaken using a finite volume CFD package. Results of this analysis which considered the conductive, convective and radiative heat exchange processes taking place in the interior of the smart window system as well as the heat exchange to the internal and external ambient environment are presented.

© 2014 The Authors. Published by Elsevier Ltd. This is an open access article under the CC BY license (http://creativecommons.org/licenses/by/3.0/).

Keywords: Smart windows; Photovoltaic; Facades; CFD

1. Introduction

Solar energy is increasingly being recognised as one of the main substitutes for fossil fuels due to its essentially non-polluting inexhaustible nature. Photovoltaic/thermal (PV/T) solar collectors, first proposed by (Kern and Russell, 1978), yield a higher utilisable energy output per unit collector area (Tripanagnostopoulos et al., 2007; Vats and Tiwari, 2012). The approach of combining a thermal and PV component is considered more appropriate for concentrating solar systems in which heat removal from the PV cells will be a critical issue. employed in buildings to provide increased thermal comfort while lowering space heating and cooling energy consumption (Safer et al., 2005a). Solar radiation is comprised of both long and short wave radiation, i.e., heat and light. When seeking to regulate the amount of solar radiation entering into a building, the challenge is to achieve desired levels of daylight intensity without excess introduction of the concomitant heat. Excessive direct solar insolation in the interior space, workplace or home, can lead to discomfort due to high levels of glare when the sun is directly in the field of view or is specularly reflected from indoor surfaces (Kim et al., 2009; Piccolo and Simone, 2009) and should be avoided. Blinds are frequently used within such façades to control the intensity of the incident direct solar radiation component by

Currently different types of double-skin façades are

http://dx.doi.org/10.1016/j.solener.2014.02.016 0038-092X/© 2014 The Authors. Published by Elsevier Ltd.

This is an open access article under the CC BY license (http://creativecommons.org/licenses/by/3.0/).

^{*} Corresponding author at: Physics Dept., College of Applied Science, Umm Al Qura University, Makkah, Saudi Arabia. Tel.: +966 (0) 566627680.

E-mail address: Mohamed.ma.sabry@gmail.com (M. Sabry).

Nomenclature

$egin{array}{c} D_h \ D_v \ D_{vc} \ d_e \ d_i \end{array}$	depth of horizontal window segment (m) depth of vertical window segment (m) depth of the differentially heated vertical cavity (m) external tube diameter (m) internal tube diameter (m)	h _{ctube} h _{cwater} W _h W _v X	tube-air heat transfer coefficient $(Wm^{-2} K^{-1})$ water-tube heat transfer coefficient $(Wm^{-2} K^{-1})$ width of horizontal window segment (m) width of vertical window segment (m) optical concentration ratio
H_h	height of horizontal window segment (m)	Greek s	ymbols
H_v	height of vertical window segment (m)	η_{cell}	solar cell electrical efficiency
H_{vc}	height of the differentially heated vertical cavity	$\mu_{ au}$	turbulent viscosity (Pa s)
	(m)	ρ_{cell}	solar cell reflectivity
h _{cback}	heat transfer coefficient of back window pane	$ ho_g$	reflectivity of window pane
	$(Wm^{-2} K^{-1})$	ρ_{lens}	reflectivity of Fresnel lens
h_{ccell}	heat transfer coefficient of solar cell	ρ_{tube}	reflectivity of copper tube
	$(Wm^{-2} K^{-1})$	τ_{cell}	solar cell transmissivity
h _{cfront}	heat transfer coefficient of front window pane	τ_g	transmissivity of window pane
	$(Wm^{-2} K^{-1})$	τ_{lens}	transmissivity of Fresnel lens
h _{clens}	heat transfer coefficient of Fresnel lens	τ_{tube}	transmissivity of copper tube
	$(Wm^{-2} K^{-1})$		

blocking the radiation from entering the building and thus reducing the cooling loads. However, these do not use the intercepted solar energy. A smart window, illustrated in Fig. 1, aims to control and regulate solar energy influx through such double skin façades to the interior of buildings. Glass coated with thin films that can change their optical properties reversibly from transparent to opaque when heated and cooled (Bange, 1999), or when subject to an applied electrical current are of great interest (DeForest et al., 2013), again however they do not utilise the incident solar energy for electricity production.



Fig. 1. A conceptual arrangement of a smart window showing its operation.

We examine a new concept of smart windows whereby water cooled concentrator-PV cell units are incorporated inside the gap between two panes of a double glazed window. Two-axis tracking Fresnel lens concentrators coupled to actively cooled high efficiency PV cells have been simulated.

Optical concentration ratio is defined as the ratio between the aperture area to the collector area, while the effective concentration ratio is calculated taking into account the reflection from both aperture and collector surfaces. PV cells considered in this study are the Quantum Well (QW) square solar cells, having area of 16 mm² which were reported to achieve efficiency of \sim 32% under an effective concentration ratio of 500× (Adams et al., 2011; Rohr et al., 2006). The variation of the cell efficiency with concentration ratio is shown in Fig. 2.

When incorporated into a double skin building façade, a point focus or linear Fresnel lens will separate the direct (beam) solar radiation from the diffuse component and concentrate the former on the solar cell whilst facilitating the passage of diffuse radiation into the interior of buildings. Such multifunctional smart windows are able to (i) generate electricity, (ii) block direct sunlight with consequent reduction in building energy cooling load, (iii) transmit diffuse sunlight to provide natural daylight and (iv) provide domestic hot water.

The following system parameters need to be optimised to achieve maximum thermal, optical and electrical performance:

• The optical concentration ratio that provides the best solar to electrical conversion efficiency of the solar cell, taking into account the reduction in performance that results from increased operating temperature. Download English Version:

https://daneshyari.com/en/article/7938319

Download Persian Version:

https://daneshyari.com/article/7938319

Daneshyari.com