



# A CALPHAD assessment of the Al–Mn–C system supported by *ab initio* calculations

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## ABSTRACT

frequently toggled from 1The Al–Mn–C ternary system has been thermodynamically evaluated using the CALPHAD method. Published data on phase equilibria have been critically examined and used to optimize the model parameters. The phase model for the  $\kappa$  AlMn<sub>3</sub>C phase (E2<sub>1</sub>) has been changed to (Al,Mn)<sub>1</sub>(Al,Mn)<sub>3</sub>(C,Va)<sub>1</sub> for improved reproduction of stability ranges and phase equilibria at 1100 °C and 1200 °C. The solid solution phase parameters of  $\gamma$ -Mn,  $\epsilon$ -AlMn,  $\epsilon$ -Mn<sub>4</sub>C have been adjusted to reproduce experimental ternary phase equilibria. Density functional theory-based *ab initio* calculations of enthalpies of formation at 0 K were performed to guide the modeling of the  $\kappa$  phase and elucidate general energetic trends. Reasonable liquidus temperatures were achieved by adjustments to the stability of the liquid phase. The Mn<sub>5</sub>C<sub>2</sub> phase model was extended to Mn<sub>5</sub>(C,Al)<sub>2</sub> which allows aluminium on the carbon sublattice. The CALPHAD calculations were performed with the optimized set of parameters and compared with the available experimental data and changes to previous work were elucidated.

## 1. Introduction

The quaternary Al–Fe–Mn–C system is the fundamental system for high manganese steels (HMnS). The current generation of advanced high strength steels (AHSS) employs complex microstructural and processing features such as twinning induced plasticity (TWIP), transformation induced plasticity (TRIP) and additionally precipitation of the  $\kappa$  phase (Fe,Mn)<sub>3</sub>AlC [1,2]. Typically, these microstructural features and mechanisms are activated by different processing routes and variation of alloying content [3]. Both the selection of the alloying content as well as crucial processing parameters such as heat treatment temperatures can be found with the help of thermodynamic calculations employing the CALPHAD method. The Al–Mn–C system is a crucial subsystem of the main quaternary system and therefore demands attention if the quaternary system is to be modeled realistically.

Schuster and Nowotny [4] suggested isothermal sections at 700 °C and 1000 °C after experimental investigations via X-ray diffraction (XRD) and light optical microscopy (LOM) on annealed and quenched samples. They reported the existence of the ternary AlMn<sub>3</sub>C compound with anti-perovskite CaTiO<sub>3</sub> structure. After that, no further

experimental determination of phase constitution was performed until the recent works by Bajenova et al. [5,6] provided isothermal sections at 1100 °C and 1200 °C as well as experimental information about the liquidus surface in the Mn-rich region of the ternary systems by differential thermo-analysis (DTA), XRD, scanning electron microscopy (SEM) and electron probe microanalysis (EPMA).

Some additional interest of research has been directed towards a metastable ferromagnetic tetragonal phase (referred to as  $\tau$ ) with less than 2 wt% C and about 70 wt% Mn for its magnetic properties [7–12]. It can be formed after isothermal annealing of  $\epsilon$ -AlMn by martensitic transition to its L1<sub>0</sub> tetragonal structure and is formed by subsequent quenching [13,14]. Due to the low alloying range and metastable phase constitution these works can not be considered useful for the assessment of the Al–Mn–C ternary system.

Even though the chemical and thermodynamic similarities of iron and manganese rightfully suggest a general similarity of the Al–Fe–C and Al–Mn–C systems, considerable differences can nonetheless be found, e.g. concerning the  $\kappa$  phase. For this phase a considerably different range of solubility and constitution can be found in the Al–Mn–C system in addition to a congruent melting point which can not be observed in Al–Fe–C.

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