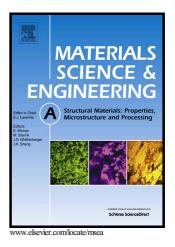
## Author's Accepted Manuscript

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### Cyclic Deformation and Microcrack Initiation During Stress

#### **Controlled High Cycle Fatigue of a Titanium Alloy**

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#### **Abstract:**

Cyclic plastic deformation, slip characteristics and crack nucleation in Ti-6Al-2Sn-2Zr-3Mo-1Cr-2Nb-0.1Si (TC21) with different morphologies of equiaxed and lamellar  $\alpha$  phase were systematically analyzed during high-cycle fatigue. The heterogeneous plastic deformation could take place within different  $\alpha$  morphologies during high-cycle fatigue even though the cyclic stress amplitude is much less than yield strength. Slip is the dominant deformation mode in the equiaxed primary  $\alpha$ ,

while the slip and  $(10\overline{1}1)$  deformation twin are prevalent in the primary  $\alpha$  lath.

Interactions between slip, twin and interface result in ledges at the primary  $\alpha$  lath interface. The relationship between cyclic slip irreversibility, accumulated irreversible strain, and fatigue life is established. A critical parameter, accumulated irreversible strain per area in the crack initiation region (region I), was calculated to be  $(8.1\pm2)\times10^{-4}$ ·µm<sup>-2</sup> for initiating fatigue crack. Fatigue cracks will nucleate when the accumulated irreversible strain exceeds the critical value. The primary  $\alpha$  lath is the dominant site for crack initiation. The cracks initiate and propagate in interface and slip band, and easily connect each other in the primary  $\alpha$  lath. In comparison, most cracks lie within an individual or occupy several equiaxed  $\alpha$  phases and often cease in front of the phase boundary, which delays the connection of microcracks. It indicates that the primary  $\alpha$  lath is more detrimental than the equiaxed primary  $\alpha$  phase during high cycle fatigue.

**Keywords:** Titanium alloy; High–cycle fatigue; Slip irreversibility; Fatigue crack initiation

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