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# Strength-ductility paradox in a directionally solidified nickel base superalloy

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#### 1. Introduction

Nickel base superalloys are microstructurally designed for use in high temperature structural applications such as in the hot sections of aircraft gas turbine engines [1,2]. The main feature of their microstructure is the dispersion of precipitates that have ordered L1<sub>2</sub> crystal structure and are coherently embedded in a solid solution strengthened  $\gamma$  matrix [2]. Due to presence of these ordered precipitates,  $\gamma'$ , nickel base superalloys exhibit typical tensile behaviour known as yield strength anomaly (YSA), which consists of an increasing or constant value of yield strength (YS) over a range of temperatures [3–4]. It is usually observed that increase in yield strength owing to YSA is accompanied by decrease in ductility of the superalloys, and the reasons for reduced ductility are different for different alloys [3–6].

However, in the present study it is observed that the alloy CM 247 DS LC exhibits enhanced ductility at 750 °C, where the yield strength of the alloy is highest. Such type of strange behaviour, where both high yield strength and high ductility occurs together is termed as strength-ductility paradox. CM 247 DS LC is a directionally solidified (DS) nickel base superalloy used for manufacturing of turbine blades and vanes. This alloy has multiphase microstructure consisting of  $\gamma'$  precipitates embedded in  $\gamma$  matrix, carbides, and  $\gamma$ - $\gamma'$  eutectics [7]. In the present investigation, the

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#### ABSTRACT

In contrast to other structural alloys, yield strength of nickel base superalloys either remains constant or increases with temperature up to 700–800 °C making them more suitable for high temperature structural applications. However, the increase in yield strength is usually accompanied by a decrease in ductility. The results of the present investigation describe the substrural evolution in a directionally solidified nickel base superalloy CM 247 DS LC during tensile deformation, where ductility is not impaired even when yield strength is highest (at 750 °C). Extensive TEM studies offer plausible dislocation based mechanisms for retention of high ductility at 750 °C. The highest yield strength is attributed to the presence of intersecting faults along with partials bounded by anti-phase boundary. However, high ductility is due to the formation of SISF inside  $\gamma'$  precipitates. These mechanisms provide necessary impetus for further alloy development.

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micromechanism of tensile deformation of alloy CM 247 DS LC at 750 °C is studied and an attempt has been made to understand the strength-ductility paradox behaviour based on the sub structural evolution. This study will be beneficial for future alloy development and improving the mechanical behaviour of alloy at elevated temperatures.

#### 2. Material and methods

The nominal composition of the alloy is listed in Table 1. The development and processing of the superalloy CM 247 DS LC is reported in [8]. The alloy was received in the form of rods of 14 mm diameter and 135 mm length with rod length parallel to the DS direction. The rods were heat-treated in the following sequence: 1221 °C/2h/1232 °C/2h/1243 °C/2h/1250 °C/2h/ gas fan quenching (GFQ), followed by aging at 1080 °C for 4 h (GFQ) and 870 °C for 20 h (GFQ).

Tensile tests were conducted in the temperature range 25–955 °C employing a strain rate of  $1 \times 10^{-3} \text{ s}^{-1}$  on round shaped threaded specimens fabricated in accordance with ASTM E 8 M in INSTRON 8862 series servo electric testing machine of load capacity 100 KN and equipped with resistance furnace. The temperature during test was controlled by a 3-zone Eurotherm PID temperature controller. During test, constant temperature within ± 2 °C was maintained in all the 3 zones. The temperature on the test piece was measured with two Pt-13%Rh thermocouples tied to the gauge length portion. Strain measurements were made using a high temperature



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Table 1 Chemical composition (wt %) of the as-received CM 247 DS LC alloy.

Ni	Cr	Со	Мо	Ti	Al	Ta	W	В	Zr	Hf	С
62	8	9.3	0.49	0.74	5.58	3.21	9.49	0.018	0.009	1.41	0.07

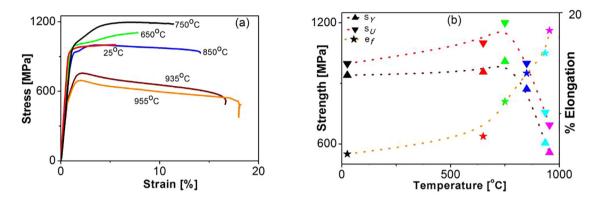
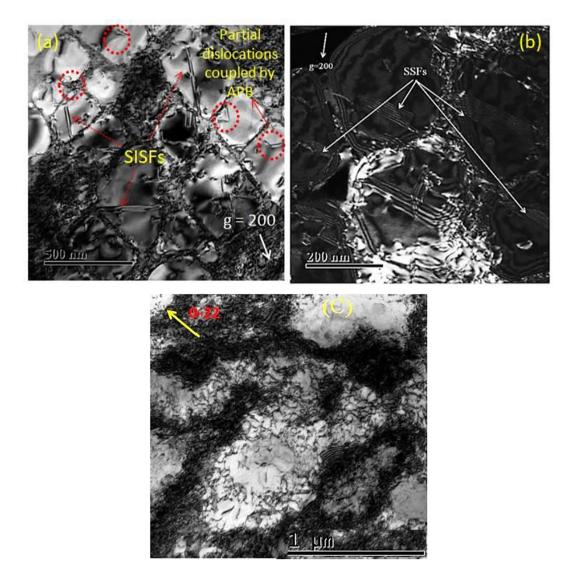


Fig. 1. (a) Typical engineering stress-strain curves and (b) Variation of S<sub>Y</sub>, S<sub>U</sub> and e<sub>f</sub> of alloy CM 247 DS LC at different tensile test temperatures.



**Fig. 2.** (a) TEM bight field image showing intense dislocation activities inside  $\gamma'$ -precipitates, superlattice intrinsic stacking faults (SISFs) and superpartial dislocations bounded by APB in the specimen and (b) TEM dark field image showing various superlattice stacking faults (SSFs) intersecting each other inside  $\gamma'$ -precipitate in the specimen tensile tested at 750 °C, and (c) TEM image of the specimen tensile tested at 850 °C.

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