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# The effects of bed form roughness on total suspended load via the Lattice Boltzmann Method

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#### ABSTRACT

Bed forms in natural rivers and man-made channels provide the dominant contribution to overall flow resistance and hence significantly affect sediment transport rate. Many laboratory experiments and field observations have been conducted on bed forms, and it was found that theoretical flat-bed assumptions do not give the correct estimation for the total suspended load (TSL). In this study, we present a systematic numerical investigation of turbulent open-channel flows over bed forms using the Lattice Boltzmann Method (LBM). A static Smagorinsky model is incorporated into LBM to account for turbulence, and the dynamic interface between fluid and air is captured by a free-surface model. The timeaveraged flow velocity, turbulence intensity and Reynolds shear stress in LBM simulations show an excellent agreement with the available experimental data. In addition, the coherent flow structures induced by the bed forms qualitatively agree with previous numerical results from Large Eddy Simulations based the Navier-Stokes equations. We then proceed to investigate the effects of bed form roughness, quantified by the total friction factor  $f_T$ , on sediment transport. It is found that the prediction of the TSL based on the theoretical flat-bed assumptions may lead to an overestimation of up to 30%, depending on the bed form roughness. In addition, the normalized TSL is linearly proportional to  $f_T$  and nearly inversely proportional to the ratio of downward settling velocity and upward turbulence induced diffusion. Our work proposes a general law linking these quantities to estimate the TSL, which has the potential for a more efficient and accurate engineering design of man-made channels and improved river management.

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#### 1. Introduction

Bed forms are present in nearly all fluvial channels and play an important role in dictating flow resistance, sediment transport and deposition. The presence of bed forms may alter the flow field and consequently affect the sediment transport in suspension. Generally, the strong wakes resulting from flow separation behind each bed form element will lead to an increase in the overall turbulence levels, and hence an extra turbulence induced diffusion that is able to enhance the flow capacity to carry sediments in suspension [1]. The increase of suspension concentration is one of the major sources of water pollutants which may harm the aquatic ecology [2]. Therefore, an in-depth study of the relationship between bed forms and sediments in suspension is of vital importance both in economy and in ecology.

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Notation	
u, v	instantaneous flow velocities in $x$ - and $y$ -direction
$\bar{u}, \bar{v}$	time-averaged flow velocities in $x$ - and $y$ -direction
u', v'	velocity fluctuations in $x$ - and $y$ -direction
u <sub>sd</sub> , v <sub>sd</sub>	turbulence intensities in x- and y-direction
$ au_{Re}$	Reynolds shear stress $(-\rho u'v')$
$\rho$	fluid density
С	sediment concentration
$\mathbf{u}_p$ $\boldsymbol{\varepsilon}$	velocity of the suspended sediments diffusivity tensor of the sediments
w	settling velocity of the sediments
х, у	streamwise and wall-normal directions
$\boldsymbol{\varepsilon}^m$	momentum diffusivity tensor
γ	proportionality between $\boldsymbol{\varepsilon}$ and $\boldsymbol{\varepsilon}^m$
$f_i$	density distribution function in the <i>i</i> th direction
Х	position of the lattice cell
$\mathbf{c}_i$	lattice speed in the <i>i</i> -th direction
$\delta_t$	time step
t T	simulation time relaxation coefficient
${ au_0 \over f_i^{eq}}$	equilibrium density distribution function
u u	fluid velocity
р	fluid pressure
C <sub>S</sub>	lattice speed of sound
Re	Reynolds number
L <sub>lu</sub>	characteristic length in lattice units
U <sub>lu</sub>	characteristic velocity in lattice units
$v_0$	fluid kinematic viscosity in lattice units
V <sub>total</sub>	total fluid viscosity in lattice units turbulence eddy viscosity in lattice units
${{ u }_{eddy}} \  au_{total}$	effective relaxation time
$C_{\rm s}$	Smagorinsky constant
$\Delta$	filtered length of the Smagorinsky model
S	large eddy strain rate tensor
$\alpha, \beta$	spatial indices
$\pi^{neq}_{lphaeta}$	sum of the second-order moments of the nonequilibrium $f_i$
Π	magnitude of the tensor $\pi^{neq}_{\alpha\beta}$
η	fluid fraction of a lattice cell
m	fluid mass inside a lattice cell
$\rho_A$ <b>n</b>	density of the gas phase surface normal vector
ĸ	small offset for cell type conversion
L	resolution of the cavity flow or the periodic length of the bed forms
U	velocity of the upper boundary in the cavity flow or mean flow velocity
$h_w$	height of the residual water column
X <sub>W</sub>	advance of the collapsing water column
H <sub>i</sub> , L <sub>i</sub>	initial height and length of the water column
L <sub>r</sub> , L <sub>t</sub> L <sub>e</sub>	lengths of the recirculation region and the flume distance between the entrance and the measured section
Le h	height of the bed form element
H	mean depth of the fluid flow
μ, σ	mean value and standard deviation
<i>u</i> *	total shear velocity
Fr	Froude number
g	gravitational acceleration
S W	slope of the inclined open channel width of the open channel
* *	when of the open channel

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