

## **Research** Paper

# Optimisation of the design of pressurised irrigation systems for irregular shaped plots



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Keywords: Irrigation Water-energy nexus Pressurized irrigation system Total water application cost Efficiency A software tool has been developed to support decision-making in optimising the design of pressurised irrigation systems (sprinkler and drip irrigation) for agricultural fields with sub-plots of any shape or topography. The tool determines the design with minimum total water application cost ( $C_T$ ) (investment + operation). This study analysed the effect of field size, shape and slope on  $C_T$  and emission uniformity (EU) for drip irrigation systems for almond and pepper, as well as two possible layouts for a maize crop for permanent sprinkler irrigation systems. The minimum  $C_T$  design used polyethylene lateral pipes of 13.6 mm internal diameter at 250 kPa for drip irrigation and polyvinylchloride pipes of 46.4 mm internal diameter at 600 kPa for the permanent sprinkler irrigation systems, except in certain cases of where there were triangular plots. In the drip irrigation fields, which were more irregularly shaped and had the largest plots, the lowest  $C_T$  was achieved with regulated flow emitters which in this study had an emission exponent x = 0.1. This was due to their increased efficiency and therefore decreases volume requirements. The use of pressure compensating drippers is recommended for large sub-plots (>1.5 ha in the analysed cases) with irregular shape and large slopes. Under the conditions studied, the 15  $\times$  15-m layout had a slightly lower C<sub>T</sub> than the 18  $\times$  18-m layout because it had greater uniformity and its increased irrigation efficiency reduced water consumption, despite having somewhat higher energy consumption and investment requirements than the  $15 \times 15$ -m layout.

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### 1. Introduction

To support the sustainable intensification of agriculture, there is a need for low-cost, reliable, efficient irrigation systems supported by policies that recognise the trade-offs between saving water, reducing  $CO_2$  emissions and intensifying food production (Daccache, Ciurana, Rodriguez Diaz, Knox, 2014). Consequently, optimal irrigation, from a sustainable point of view, can only be achieved by simultaneously considering environmental and economic criteria. Thus, it is necessary to develop tools and models that can contribute directly to improving water and energy use in irrigation through a holistic approach for irrigation design and management.

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Nomenclature	K emission coefficient
ANOVA analysis of the variance	K <sub>s</sub> emission coefficient of the sub-system
AP average application rate (mm $h^{-1}$ )	L pipe length (m)
$AK_a$ average application rate (mm m)	N useful life (year)
$C_a$ investment annulty ( $\in$ na year)	N <sub>p</sub> power required (kW)
$C_e$ energy annulty ( $\in$ na year )	O <sub>t</sub> annual operating time of the irrigation system
$C_i$ investment costs ( $\in$ )	(h year <sup>-1</sup> )
$C_m$ maintenance annuity ( $\in$ na <sup>-</sup> year <sup>-</sup> )	p p-value
CRF capital recovery factor $(a_1 - 1)$	PE polyethylene
$C_{\rm T}$ total water application cost ( $\in$ ha <sup>-1</sup> year <sup>-1</sup> )	PRESUD pressurised sub-plot design
CUC Christiansen's uniformity coefficient	PRESUD-IR pressurised irregular sub-plot design
$CV_h$ coefficient of variation of pressure head	PVC polyvinylchloride
$CV_q$ coefficient of variation of the flow rate in the	$P_w$ irrigation water price ( $\in m^{-3}$ )
Subunit	$Q_0$ flow rate of the pipe (m <sup>3</sup> s <sup>-1</sup> )
$Cv_{qh}$ coefficient of variation of emitter flow due to	$q_a$ average emitter discharge (l h <sup>-1</sup> )
pressure variations	$q_e$ emission flow rate of the emitter (l h <sup>-1</sup> )
CV <sub>qmf</sub> manufacturer coefficient of variation of the	$q_{ei}$ emission flow rate for one emitter (l h <sup>-1</sup> )
$C = \frac{1}{2} \sum_{n=1}^{\infty} $	$q_{mh}$ minimum emitter flow in the plot (l h <sup>-1</sup> )
$C_w$ water cost annuity ( $\in$ na year )	$Q_s$ flow rate at the plot intake (m <sup>3</sup> s <sup>-1</sup> )
D Internal pipe diameter (mm)	R search radius (m)
$DE_a$ distribution efficiency	R <sup>2</sup> coefficient of determination
$D_{rs}$ gross average water depth that reaches the solic surface (m <sup>3</sup> ha <sup>-1</sup> year <sup>-1</sup> )	R <sub>e</sub> fraction of applied water that reaches the soil
e number of emitters per plant	surface
E <sub>c</sub> general application efficiency for the irrigation	$R_g$ gross water requirement (m <sup>3</sup> ha <sup>-1</sup> year <sup>-1</sup> )
system	$R_n$ net crop irrigation water requirement
En energy rate ( $\in kWh^{-1}$ )	$(m^3 ha^{-1} year^{-1})$
$E_n$ efficiency of the pumping system	S irrigated area (ha)
EU emission uniformity	S <sub>0</sub> slope of the plot (%)
f friction factor of Darcy–Weisbach equation	$s_e$ emitter spacing along the lateral pipe (m)
$H_0$ pressure head value at the subunit intake	s <sub>l</sub> lateral pipe spacing (m)
$(m kPa^{-1})$	Tr peak-use period transmission ratio
$h_a$ average pressure head in the system (kPa)	x emission exponent
$h_e$ intake pressure head of the emitter (m)	$\Delta h$ difference in pressure heads in the irrigation plot
$h_{ei}$ pressure head for each emitter (m)	
h <sub>f</sub> friction losses (m)	$\Delta q$ anterence in emitter now in the irrigation sub-plot
i annual interest rate	(%)
Jn number of emitters to miss out	

The main aspects of the design and management of an irrigation system are maximising water application uniformity, minimising drift and evaporation losses, and estimating the telemetry requirements whilst reducing maintenance costs at a minimum. It is important to consider the emission uniformity (*EU*), investment and energy costs, crop response to water application uniformity (yield decreases due to nonuniform irrigation), and gross margin, among other variables. The first three variables were used to calculate the irrigation water application cost.

Solomon (1984) reported that a lack of uniformity in micro irrigation plots is mainly caused by: emitter ageing and clogging, the number of emitters per plant (e), the manufacturer coefficient of variation of the emitters ( $CV_{qmf}$ ), pressure head variation due to differences in ground elevation and head losses in the pipes, and variations in the emission exponent (x).

Warrick and Yitayew (1988) presented several graphs for determining the length and diameter of lateral pipes and

the intake head assuming a specific average emitter flow and water application uniformity. Kang, Yuan, and Nishiyama, 1999 developed a method for designing micro irrigation lateral pipes at a minimum cost based on the design methods of finite elements and golden-section searches. Some of the main characteristics of the system, such as lateral pipe diameters and lengths, were analysed considering uniformly and non-uniformly sloped fields. Hassanli and Dandy (2000) applied genetic algorithms to develop hydraulic calculations and designs for rectangular drip irrigation units. Zayani, Alouini, Lebdi, and Lamaddalena (2001) developed a method to design multiple outlet pipes under relatively constant outflow using the energy drop ratio approach and analytical methods. Juana, Rodríguez-Sinobas, Sánchez, and Losada (2005) developed analytical expressions relating water distribution indexes to design variables that define trapezoidal drip irrigation plots. Zayani, Hammami, Alouini, and Souissi (2013) developed an analytical method to design evenly sloping drip irrigation

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