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# Development and experimental validation of a multi-algorithmic hybrid attitude determination and control system for a small satellite

Dae Young Lee<sup>a</sup>, Hyeongjun Par<sup>b,\*</sup>, Marcello Romano<sup>c</sup>, James Cutler<sup>d</sup>

<sup>a</sup> Center for Space Research, University of Texas, Austin, TX, USA

<sup>b</sup> Mechanical and Aerospace Engineering, New Mexico State University, Las Cruces, NM, USA

<sup>c</sup> Mechanical and Aerospace Engineering, Naval Postgraduate School, Monterey, CA, USA

<sup>d</sup> Aerospace Engineering, University of Michigan, Ann Arbor, MI, USA

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## ABSTRACT

Advanced missions of satellites are increasingly demanding more accurate and robust attitude maneuvering capabilities. However, it is difficult to achieve especially for small satellites due to limited hardware resources of sensors, actuators, and processors. In this paper, to achieve the desired performance, a multi-algorithmic hybrid attitude determination and control system (ADCS) that utilizes a family of control and estimation algorithms is developed and implemented in numerical simulations and experiments for a small satellite. The hybrid automaton framework of the ADCS is designed to accomplish the desired performance with the limited hardware capability by switching the control and estimation algorithms effectively for given situations in space. The performance of the hybrid ADCS is evaluated through numerical and hardware-in-the-loop simulations that are based on a three-dimensional air-bearing testbed, CubeSat Three-Axis Simulator (CubeTAS). Simulation and experimental results demonstrate the effectiveness of the multi-algorithmic hybrid ADCS. The significance of this paper is in demonstrating that the hybrid automaton framework can be an effective approach to handle operational situations in space. It also provides a design reference for a small satellite ADCS.

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## 1. Introduction

With the increasing application of small satellites, there exist massive and concurrent requests for extensive functions and capabilities such as higher pointing accuracy or maximum power generation [1]. One representative of these requests is an extension in attitude maneuvering capability from passive stabilization to active attitude control. The passive magnetic stabilization methods with a permanent magnet and hysteresis strips only guarantee nadir pointing in a specific orbit region [2]. This method is simple to design and easy to build, and does not even require on-orbit calculation or management. However, this is not precise enough to conduct reconnaissance on a specific area, environmental monitoring, and communication with a specific ground station. These popular and advanced missions can only be achieved with an active ADCS for agile maneuvering in orbit, which is a challenging task not only for a small satellite but also for a large satellite.

In the early stage of small satellite development, rough nadir pointing with magnetic devices was used for missions, but recent missions often require less than a few degrees of pointing accuracy with the use of a reaction wheel assembly (RWA), magnetorquer, and even paired thrusters. This trend is found in the project history of several universities and research institutes that have conducted multiple satellite missions successfully. For example, all the missions from the Michigan eXploration Laboratory (MXL) at the University of Michigan [3–6], the Delfi series from the Delft University of Technology (TU Delft) [7,8] and the CAN-X series of the University of Toronto [9] present similar ADCS development trends. Each of them has started only with passive stabilization, then they have transferred to more complex active ADCS development as their experiences and know-how of spacecraft attitude managing have been accumulated from the early stage missions. A survey of the attitude control method for each individual launched CubeSat mission is provided in [10].

The limited resources, such as small actuators, low-cost sensors, and low-powered processors, and operational capability make active ADCS of a small satellite difficult. For example, small-sized reaction wheels that are popular in a small satellite design experience an easy saturation of angular momentum due to disturbance torques in Low Earth Orbits (LEO). In such a case, stability or

\* Corresponding author.

E-mail addresses: daylee@utexas.edu (D.Y. Lee), htpark@nmsu.edu (H. Par), mromano@nps.edu (M. Romano), jwcutler@umich.edu (J. Cutler).

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1 pointing accuracy of the spacecraft could be lost. To prevent this, 2  
3 a magnetic control device and algorithm is required as a comple- 68  
4 ment for an RWA. The implementation of the magnetic control, 69  
5 however, degrades the pointing accuracy of a satellite due to the 70  
6 objective conflict between the required algorithms. Another chal- 71  
7 lenge in the active ADCS takes place when an Extended Kalman 72  
8 Filter (EKF) [11] is used for on-orbit attitude determination. A large 73  
9 error in the initial estimation may cause divergence in the attitude 74  
10 estimation due to the linearization-based characteristics of the EKF 75  
11 [12]. Consequently, in practice, simpler estimation algorithms, such 76  
12 as QUaternion ESTimation (QUEST) [13,14] and TRIAD [15,16], are 77  
13 implemented prior to activating the EKF to reduce the initial esti- 78  
14 mation error. A condition to switch from QUEST to EKF, therefore, 79  
15 should be selected carefully [3], similarly with the switching of 80  
16 the control algorithms. These challenges demonstrate that the de- 81  
17 velopment and implementation of multi-algorithmic control and 82  
18 estimation are essential in an active ADCS. 83

19 Active ADCS approaches for small satellites have been stud- 84  
20 ied and developed by several research groups. The Space Flight 85  
21 Laboratory (SFL) at the University of Toronto developed an active 86  
22 ADCS algorithm for CanX-2 that performed successful attitude esti- 87  
23 mation and pointing with sensors and miniature wheels in space 88  
24 [17]. CanX-4 and CanX-5 of SFL achieved in-orbit demonstrations 89  
25 of formation flight by ADCS with three reaction wheels mounted 90  
26 orthogonally [18]. Through the Delfi nanosatellite program of the 91  
27 TU Delft, the Delfi-n3Xt satellite has been developed and tested 92  
28 in space with a highly integrated ADCS that performs three-axis 93  
29 active control using reaction wheels [19]. The Institute of Space 94  
30 Research of the Russian Academy of Sciences has developed the 95  
31 Chibis-M microsatellite ADCS using six reaction wheels and three 96  
32 magnetoquers as a demonstration with redundant actuators [20]. 97  
33 The ADCS was validated through the laboratory tests and in-orbit 98  
34 flight. A one-unit small satellite, ESTCube-1, was developed by the 99  
35 University of Tartu. It utilized the spin rate control algorithm to si- 100  
36 multaneously align the spin axis with the Earth's inertial reference 101  
37 frame using only electro-magnetic coils [21]. Its algorithm was ver- 102  
38 ified to achieve a pointing error less than 3 deg by implementing 103  
39 numerical simulations. 104

40 In this paper, we propose an autonomous active ADCS that 105  
41 exploits multiple control and attitude determination algorithms 106  
42 based on a hybrid automaton framework to achieve high pointing 107  
43 accuracy. Pre-developed control and estimation methods are mod- 108  
44 ified and merged into the proposed hybrid automaton framework. 109  
45 Realistic operation scenarios in orbit are assumed and simulated 110  
46 on a numerical simulator. The hybrid automaton framework is also 111  
47 experimentally validated on an air-bearing testbed. Motivated by 112  
48 the importance of ground testing and verification of ADCS algo- 113  
49 rithms, an experimental air-bearing testbed, CubeSat Three-Axis 114  
50 Simulator (CubeTAS) [22–24], has been developed to simulate a 115  
51 frictionless and torque-free environment. The CubeTAS hardware- 116  
52 in-the-loop (HIL) simulator consists of a hemispherical air bearing 117  
53 in which contains the sensors, actuators, computers, and power 118  
54 storage. The developed hybrid ADCS using multiple algorithms is 119  
55 implemented in the embedded system of CubeTAS to verify the 120  
56 maneuvering performance with real sensors, actuators, and com- 121  
57 puting resources. 122

58 While there are not many references about active ADCS for 123  
59 CubeSat from the design stage to the final ground validation stage, 124  
60 this paper provides the design and validation process including 125  
61 design requirements and the related considerations, a theoret- 126  
62 ical approach to the hybrid control, system implementation, and 127  
63 experimental validation methods and procedures on the ground. 128  
64 An important contribution of this paper is experimentally validat- 129  
65 ing the hybrid system's framework for multi-algorithms using the 130  
66 three-axis air-bearing test bed. To the best of our knowledge, there 131  
are no research papers on the validation of multi-algorithms for a 132

small satellite in the three-axis air-bearing test facilities. In this 67  
research, we validate the attitude determination and control algo- 68  
rithm through the hardware-in-the-loop-simulations. Secondly, we 69  
provide the definition of modes and jump conditions in the hybrid 70  
system theory. This has not been reported in the research com- 71  
munity related to CubeSat although this is crucial for designing a 72  
multi-mode algorithm to avoid mission failures and early, success- 73  
ful completion of CubeSat missions. What's especially crucial is the 74  
hybrid system framework targets CubeSat with the reaction wheel 75  
assembly that has an angular momentum desaturation problem. 76

77 The paper is organized as follows. The mission requirement 78  
analysis and selection of actuators and sensors are presented in 79  
Section 2. Next, main estimation and control algorithms are de- 80  
signed and analyzed in Section 3. To complement the expected 81  
limitations in various situations, auxiliary control algorithms are 82  
also developed and added. In Section 4, the developed control 83  
and estimation algorithms are integrated with a hybrid automaton 84  
framework. The hybrid automaton strategy enables various con- 85  
trol modes of the satellite to autonomously handle the situations 86  
instead of sending commands from a ground station. The hybrid 87  
automaton framework is a key enabler for autonomous and pre- 88  
cise pointing control of an active ADCS in this research. As the last 89  
stage of the design process, numerical simulations and HIL sim- 90  
ulations (HILS) are implemented to validate the multi-algorithmic 91  
hybrid ADCS in Section 5. 92

## 93 2. ADCS design process 94

95 Fig. 1 provides an overview of this ADCS design process. First, 96  
97 the satellite coordinate frames with the desired attitude and the 97  
98 pointing error range are defined based on the requirements of 98  
99 the mission. Next, actuators and sensors are selected by consid- 99  
100 ering the required pointing accuracy. Notice that reaction wheels 100  
101 need to be combined with other devices such as magnetoquers for 101  
102 the angular momentum desaturation. Main estimation and control 102  
103 algorithms are then designed and analyzed. However, a smaller 103  
104 satellite with fast initial rotating speed and low-cost hardware 104  
105 requires intermediate and complementary algorithms that can re- 105  
106 duce the uncertainty caused by the operational characteristics and 106  
107 hardware performance limitation. Therefore, these complimentary 107  
108 algorithms are also developed and implemented. One important 108  
109 contribution of this research is integrating the multiple algorithms 109  
110 using a hybrid automaton framework. Normally, various situations 110  
111 of a satellite have been handled with commands given from a 111  
112 ground station. However, using the hybrid automaton framework, 112  
113 an autonomous ADCS can be designed. Operation strategies and 113  
114 commanding sequences after the deployment in space are investi- 114  
115 gated to design the hybrid automaton. As the last stage, numerical 115  
116 simulations and experiments are conducted to validate the design. 116  
117 For the numerical simulations, a MATLAB/Simulink simulator base 117  
118 on the Lie Group Variational Integrator (LGV1) is implemented. The 118  
119 3D air-bearing testbed, CubeTAS, is used for experiments. 119

### 120 2.1. Mission requirement analysis 121

122 The first step of an ADCS design is to analyze mission re- 122  
123 quirements. During the analysis procedure, satellite body and orbit 123  
124 coordinates must be defined for measuring the pointing accuracy 124  
125 of the satellite. The coordinates that the mission requirements are 125  
126 subjective must be defined clearly. For example, in the small satel- 126  
127 lite mission of CADRE [6], capturing ions and neutral winds with a 127  
128 device is the main goal of the mission. To capture ions, the satel- 128  
129 lite with the field-of-view requires to point within 15 deg of the 129  
130 velocity vector to accomplish measurements. Moreover, in order 130  
131 to maximize captured ions, the pointing direction of the satellite 131  
132 should be within one degree angle from its orbital velocity vector

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