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Separation control by a microfabricated SDBD plasma actuator for small engine turbine applications: Influence of the excitation waveform

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ABSTRACT

Article history: Small engines will be finding increasing applications in unmanned aerial vehicles (UAVs), drones and Received 8 August 2017 helicopters. However, their turbomachines exhibit lower efficiencies than those of large scale engines. In Received in revised form 18 January 2018 this context, the aerodynamic losses in the low-pressure turbines (LPTs) are largely accountable to flow Accepted 23 January 2018 separation at low Reynolds numbers operation, i.e. in cruise conditions. Active flow control is a promising Available online xxxx technology to suppress separation, thus reducing losses, fuel consumption rates and therefore emissions. The present paper is focused on the experimental investigation of the potentialities of a Single Dielectric Keywords: Barrier Discharge Plasma Actuator (SDBDPA) to reattach the separated flow at a Reynolds number of Low pressure gas turbine $2 \cdot 10^4$. The influence of the high voltage (HV) waveform supplying the SDBDPA on both flow separation Low Reynolds number Active flow control control and device power dissipation was studied. Dielectric barrier discharge plasma actuator The investigated SDBDPA was manufactured by microfabrication techniques. Photolithography ensured Microfabrication thin metal deposition with high manufacturing reliability control. Due to the possible device degradation High voltage waveform during operation, emphasis was put in selecting thin film materials that could withstand the plasma environment. Schott alkali-free borosilicate glass substrate was chosen as dielectric, while a multilayer tungsten (W)/titanium nitride (TiN) as electrode material. The experimental approach comprised the actuator testing over a curved wall plate, designed with a shape to reproduce the suction surface of a LPT and installed in closed loop wind tunnel test section. The SDBDPA was located at the front side of the adverse pressure gradient area, in order to control flow separation. Different HV excitation waveforms (sinus, triangle and square) and amplitudes were tested and compared, aiming to identify the input signal that gave the best flow control authority and device energy conversion efficiency. The applied voltage and the discharge current were acquired in order to determine the actuator dissipated power. Two-dimensional (2-D) flow velocity measurements were carried out by laser Doppler velocimetry (LDV) and particle image velocimetry (PIV). Velocity results showed that the extension of the separation area was reduced by actuation. Moreover, when the actuator was on, the boundary layer thickness and the negative velocity magnitude decreased. Their reduction increased with the applied voltage (i.e. higher power dissipations). At comparable peakto-peak applied voltages, the sinus waveforms slightly outperformed the other waveforms; however, while the sinus and triangle ones had comparable power dissipation, the square wave always dissipated the most. © 2018 Elsevier Masson SAS. All rights reserved.

1. Introduction

Aeronautical LPT blades might be subjugated to low Reynolds number flow effects due to the change in density from high altitude operation. In this circumstance, the Reynolds number can decrease below 25000. Laminar separation may thus develop on the suction surface together with the appearance of secondary flows [1], with a subsequent drop in the engine performance. The low Reynolds condition becomes even a greater issue when dealing with modern high-lift blades [2] and small/medium-sized gas turbines [3-7]. Because of the reduced size, small LPTs, used or planned to be used in small aircrafts, UAVs and drones, exhibit not only low-Reynolds numbers but also low flow rates, low component pressure ratios and high rotational speed, which lead to a further reduction in efficiency in comparison with larger size

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Fig. 1. Conceptual drawing on SDBDPAs applied on the suction surface of LPT rotor blades: absence of control (left); presence of control (right).

machines [5–7]. Counteract flow separation is thus of crucial importance.

Laminar flow separation was experimentally [3] and numerically [8] observed in a single stage axial-flow turbine, operating at a Reynolds number (based on the stator chord length and stator inlet velocity) equal to 20.000 and an inlet turbulence intensity of 0.5%. Moreover, it was also found a strong interaction of the separated flow with the secondary flows. Similar experimental investigations and findings under the same operating conditions are also found in Matsunuma et al. [9]. Secondary flows usually cause almost 30–50% of the overall loss in a blade row with a significant reduction of the LPT efficiency [10]. A nearly 300% increase in the loss coefficient was indicated for an aero-engine LPT at a Reynolds number below $2 \cdot 10^5$, primarily associated with a laminar separation over the trailing half of the blade suction surface [11].

The control of laminar separation bubbles has been subject of many studies in recent years. Several flow control techniques have been investigated with particular interest in active flow control methods [12–16].

33 Among active flow control devices, an interesting one is the 34 SDBDPA, which is cheap, easy to be implemented on a surface, 35 light in weight and high response frequency. Moreover, it is pow-36 ered with an electrical input energy that allows easy control and 37 high-bandwidth modulation of the actuation. The SDBDPAs are 38 composed of two metallic electrodes separated by a dielectric 39 layer: one electrode is supplied with a HV waveform and exposed 40 to the surrounding flow; the other one is grounded and covered 41 by insulating material. The application a voltage waveform in the 42 kV and kHz ranges (with or without modulation or pulsing) causes 43 the air near the plasma actuator to weakly ionize. The electric field 44 interaction with the charged particles results in a net body force 45 that acts on the neutrally charged air. When operating in a sepa-46 rated flow, the body force effect leads to the energization of the 47 boundary layer, which can result in its reattachment.

48 Plasma actuators have been already investigated as an effec-49 tive active control strategy in eliminating the LPT separation at 50 low Reynolds numbers [1], [11], [15–19]. Fig. 1 shows a concep-51 tual drawing on SDBDPAs applied on the suction surface of LPT 52 rotor blades. The actuators, placed approximately at the separa-53 tion location, bring to flow reattachment. However, it is important 54 to mention that these devices possess low electrical-to-fluidic en-55 ergy conversion efficiency and the effect that the external flow 56 has on the performance of the actuator itself must also be con-57 sidered [15], [20–22]. For this reason, they have primarily been 58 limited to relatively low speed (freestream velocities lower than 59 30 m/s) and low Reynolds number (of maximum a few 10^5) [23], 60 [24]. Nevertheless, claims of control authority for freestream veloc-61 ities as high as 60 m/s with Reynolds number of 10^6 have been presented in the literature [25], [26]. Among the parameters im-62 63 proving the effectiveness of the SDBDPAs, it is established that 64 changes in the geometry of the actuator (dielectric laver mate-65 rial [27], [28], thickness of the both the dielectric layer [27], [28] 66 and exposed electrode [29], electrode gap [28], grounded electrode

width and number [30], [31]), in the dielectric layer surface temperature [32] and in the electrical settings [26–28], [33–41] can be effective to significantly enhance electric wind velocity and, consequently, the resulting force production. Moreover, multiple actuator arrays could be adopted [27], [28]. However, the cost implications in terms of dissipated power should be always evaluated.

In Bernard and Moreau [37], the influence of the HV waveform 73 74 was experimentally investigated for four different signals (sine, 75 square, positive and negative ramps) supplying a SDBDPA placed 76 in initially quiescent flow conditions. Results showed that, if one 77 wants to optimally use the SDBDPAs in terms of mean force by 78 electrical power consumption, the sine waveform is recommended 79 as input voltage. Indeed, at a constant consumed electrical power, 80 a sine waveform gave the best performance. Nevertheless, at con-81 stant applied voltage or frequency, the square signal caused higher thrust, but at a price of a large consumed power. A second met-82 83 ric that determines the effectiveness of such actuator for control 84 is the mean velocity of the electric wind produced by the plasma, as well as the amplitude of the velocity fluctuations that can be 85 achieved. Always in Bernard and Moreau [37], the largest mean 86 flow velocity, at constant applied voltage and frequency, was ob-87 served for a square input waveform; this agrees with the force 88 89 measurements. The sine waveform led to a slightly smaller mean flow velocity when performances were further degraded by us-90 ing the ramp shapes (especially the positive one). However, the 91 largest fluctuations in the velocity component in the horizontal di-92 rection (i.e., direction of the plasma layer) are observed for a sine 93 waveform when they are minimized by using a positive ramp. This 94 suggested that sine waveform could be probably more effective in 95 flow separation control. Again, the amplitude of vertical velocity 96 fluctuations was increased by using a sine waveform. 97

In Jolibois and Moreau [38], the waveform of the applied voltage (sine, triangle, square, trapezium, positive and negative ramps) has also been investigated experimentally as input parameter able to influence the actuator electromechanical performance. Experimental tests were always performed in absence of external airflow. Results showed that at same electrical power consumption, the discharge induced the same maximum velocity whatever the waveform, excepted with the square and the positive ramp ones that resulted in a smaller electric wind velocity. Comparing the sinus and square waveforms, it was found that, at similar power consumption, the sine voltage induced a faster electric wind with a discharge closer to the wall than the square waveform. This might be explained by the fact that, for example, a voltage of 18 kV was needed to consume 0.75 W/cm with the sine HV whereas only 16 kV were necessary in the case of the square high voltage.

The aim of this paper was to investigate the influence of the HV waveform supplying a SDBDPA on flow separation control in a LPT at low Reynolds number. Therefore, differently from the available literature studying the role of the electric waveform (where the actuator was always placed in a quiescent flow [27], [37–39]), in the present work experiments were conducted in presence of external flow. Three different excitation signals (sine, square and triangle) were experimentally tested at fixed frequency and different amplitudes. The LPT rotor blade investigated in the works of Matsunuma et al. [1], [9], [42], [43] was considered. 2-D flow velocity measurements in presence of actuation were carried out by PIV. Simultaneously, the SDBDPA applied voltage and the discharge current flowing in the circuit were acquired in order to determine the device dissipated power. Velocity measurements in absence of actuation were also performed by PIV and LDV.

The SDBDPA materials and manufacturing procedure were carefully chosen, both influencing the actuator durability [44], [45].

Dielectric materials to be used in SDBD plasma actuator applications must possess a high dielectric strength and must not chemically degrade in the presence of the plasma [27]. In many

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