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Fatigue reliability analysis of mooring system for fish cage

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ABSTRACT

Fish cages in the open sea are exposed to cycle loads due to irregular wave climate during their service life, and thus the fatigue reliability assessment of mooring system should be conducted to ensure the safe operation. The aim of this study is to evaluate the fatigue failure probability of mooring system for fish cage. Numerical simulation of net cage in random waves is performed and the time dependent approach is applied to conduct the fatigue reliability analysis of shackle chains based on S-N curve method. The sensitivity analysis of fatigue reliability of mooring line to the uncertainty of random variables in the fatigue limit state is conducted. In addition, the system reliability for mooring system is analyzed and the effect of the initial pretension and safety factor on system reliability is investigated. The results indicate that a case without the initial pretension on anchor lines is helpful to decrease the failure probability of mooring system and the safety factor of mooring lines in the current regulation is conservative for the system reliability against fatigue damage.

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1. Introduction

Aquaculture is today the fastest growing sector of the world food industry, increasing in volume by more than 10% per year, and currently accounting for more than 35% of all fish consumed, and now it is becoming the world's largest protein source. In the past decades, the aquacultural farms have been located in sheltered waters inside the fjords, where the farms are protected from extreme weather. However, the expansion of near-shore aquaculture is becoming more difficult due to coastal multi-use issues and environmental impact concerns [1]. Thus, the fish farm is recently forced to move into the offshore area, which means that the more exposed area will be utilized and the more severe environmental load will be applied. Therefore, the future designs of fish farm must be significantly more robust than the present designs, which frequently experience the escape of fish. From an engineering perspective, the main focus will be to design a system which has an overall acceptable reliability. Time-dependent reliability analysis of mooring lines for single-cage and multi-cage system was conducted for the ultimate limit state considering the corrosion effect and the uncertainties of the significant wave height and period, and the corrosion depth of chains [2]. Although the extreme environmental event may govern the design on some occasions, the

https://doi.org/10.1016/j.apor.2017.12.008 0141-1187/© 2017 Elsevier Ltd. All rights reserved. complicated mooring system of fish farms exposed to wave loads is vulnerable to cumulative fatigue damage due to the cyclic nature of the wave loading, and the fatigue failure may occur earlier than the emergence of the extreme environmental event. Thus, for both existing and future fish farms, the integrity of the mooring system should be investigated in order to withstand the environmental cyclic loads.

Numerous numerical studies have been conducted on the hydrodynamic analysis of fish cage structures, including net panels, floating collars, net cages and mooring systems. Lader and Fredheim [3] established a numerical model using super element to investigate the dynamics properties of a flexible net sheet under the wave loads. Balash et al. [4] analyzed the steady loads on the plane net through numerical simulation, in which the net is considered as an inter-connected system of lumped masses and springs. Patursson et al. [5] modeled the net as a sheet of porous media to improve the computational efficiency and obtained the flow characteristics through and around net panel. Bouhoubeiny et al. [6] performed Time-Resolved Particle Image Velocimetry measurements to study the hydrodynamic flow interaction with fishing net structure and demonstrated the influence of fluttering net structure. Zhou et al. [7] investigated the hydrodynamic characteristics of knotless nylon netting with the variation of solidity ratio in normal, parallel and angle of incline to free stream. Kristiansen [8] analyzed fully nonlinear wave body interaction problems by numerical







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Nomenc	lature	U A
т	Tansian force	σ_B
	Flongation of mooring lines	
1	Initial length of mooring lines	
S(f)	Input wave spectrum	
З()) Н.	Significant wave height	f Y
T.	Significant wave period	
T_{n}	Spectral peak period	
f	Wave frequency	
fn	Spectral wave frequency	β
ν ν	Peak enhancement factor	X *
σ	Peak shape factor	Y *
u(x, z, t)	Horizontal velocity of water particles at time t	Φ.
w(x, z, t)	Vertical velocity of water particles at time t	
ai	Wave amplitude of <i>i</i> th component wave	$\mu_{\mathbf{x}}$
ĥ	Water depth	$\sigma_{\rm X}$
f_i	Wave frequency of <i>i</i> th component wave	E _{Xi}
k _i	Wave number of <i>i</i> th component wave	SF
ε_i	Random phase of <i>i</i> th component wave	P(0
x	Horizontal coordinate of water particles	Plo
Ζ	Vertical coordinate of water particles	Pu
р	Occurrence probability of each sea state	P(0
C_{Dj}	Drag coefficient in the direction of the <i>j</i> component,	
	$j = \tau, \eta, \xi$	β_i ,
C _{mj}	Added mass coefficient in the direction of the <i>j</i> com-	Φ(
	ponent, $j = \tau, \eta, \xi$	
Fj	External forces on the net twine for the <i>j</i> component,	ρ_{ij}
	$j = \tau, \eta, \xi$	
u _j	Fluid particle velocity vector at the element center	F
	for the <i>j</i> component, $j = \tau, \eta, \xi$	γ_f
A_j	Projected area for the <i>j</i> component, $j = \tau, \eta, \xi$	K _c
V ₀	Water displaced volume of an element	<i>v</i> ₀
R _j	Central velocity vector of element for the <i>j</i> compo-	
	nent, $j = \tau, \eta, \xi$	
u_j	Fluid particle acceleration vector at the element	
Ď	Central acceleration vector of element for the i com	
к _ј	central acceleration vector of element for the j com-	
0	$Ponent, j = i, i, j \in \mathbb{R}$	
	Viscosity of water	wave
μ (Normal drag coefficient for mesh bar	collai
C_{η}	Tangential drag coefficient for mesh bar	2 flo
V_{Pm}	Normal component of the fluid velocity relative to	elasti
· Kij	the bar	nnite
S	Stress range (double amplitude) in MPa	moor
N	Number of cycles for the stress range <i>S</i> to failure	devel fish a
Κ	Intercept parameter of S-N curve	atrop
т	Slope parameter of S-N curve	duo t
D	Accumulative fatigue damage	the h
T_L	Design lifetime	by h
$N(S_i)$	Number of cycles to failure at stress range S _i	with
$N(T_L)$	Number of stress cycles in total time T_L	respo
Α	Scale parameter in Weibull distribution	irreg
В	Shape parameter in Weibull distribution	two
v_0^+	Load cycle per unit time	Clirre
Δ	Allowable fatigue damage	the f
N(<i>e</i> , <i>sd</i>)	Normal distribution with the expected value <i>e</i> and	struc

N(<i>e</i> , <i>sd</i>)	Normal distribution with the expected value <i>e</i> and
	standard deviation sd
LN(e, sd)	Log-normal distribution with the expected value <i>e</i>
	and standard deviation sd

- H Hessian matrix
- *C*_{*A*,*B*} Covariance matrix
- ρ_{AB} Correlation coefficient of scale and shape parameters

σ_A	Standard deviation of scale parameter	
σ_B	Standard deviation of shape parameter	
$\Gamma(\cdot)$	Gamma function	
Χ	Random variables	
$z(\boldsymbol{X})$	Limit state function for variable vector X	
$P\{z(\boldsymbol{X}) \leq 0$	Probability of $z(X) \le 0$	
$f(\boldsymbol{X})$	Joint probability density function of X	
p_f	Failure probability of structures	
R	Reliability of structures	
Y	Independent variables	
β	Reliability index	
$X^* = (x_1, x_2)$) Design point in X space	
$Y = (y_1, y_2)$) Design point in Y space	
$\Phi^{-1}(\cdot)$	Inverse function of the standard normal probability	
	distribution	
μ_{Xi}	Expected value of random variable <i>X_i</i>	
σ_{Xi}	Standard deviation of random variable <i>X_i</i>	
ε_{Xi}	Important factor of random variable X _i	
SF _i	Sensitivity factor for random variable <i>X_i</i>	
$P(C_i)$	Failure probability of the <i>i</i> th component	
Plower	Lower bound for system failure probability	
Pupper	Upper bound for system failure probability	
$P(C_{ij})$	Joint failure probability of the <i>i</i> th and the <i>j</i> th com-	
	ponents	
β_i, β_j	Reliability indices for the <i>i</i> th and <i>j</i> th components	
$\Phi(\cdot)$	Cumulative probability distribution function for 1-D	
	standard normal distribution	
$ ho_{ij}$	Correlation coefficient between the <i>i</i> th and the <i>j</i> th	
	components	
F	Safety factor	
γ_f	Partial safety factor for fatigue load	
Kc	Characteristic value of K	
v_{0c}^{+}	Characteristic value of v_0^+	
B _c	Characteristic value of <i>B</i>	
Ac	Characteristic value of A	
Δ_c	Characteristic value of Δ	

tank to calculate wave loads on a floating horizontal r. Fu and Moan [9] predicted the dynamic response of 5 by ating collars by the application of an extended 3D hydrocity theory in regular waves. Huang et al. [10] developed a element model to investigate the elastic deformations and ing line tensions of floating collar in waves. Lee et al. [11] oped a mass-spring model to analyze the performance of age system in current and waves. Moe et al. [12] performed gth analysis to obtain the loads distribution in the net cage to current, weights and gravity. Xu et al. [13] investigated hydrodynamic behavior of multi-cage and mooring system umped-mass model under the action of waves combined current. Li et al. [14] analyzed the nonlinear hydro-elastic onse by finite element model of a deep-water gravity cage in ular waves. Grue [15] predicted the mooring line loads for systems of gravity net cages under the action of wave and ents through numerical simulation. Kim et al. [16] analyzed flow field characteristics within the abalone containment structure with computational fluid dynamic software and investigated the hydrodynamic response of the moored containment structure with a Morison equation type finite element model. Ito et al. [17] investigated the hydrodynamic behaviors of a cubic shaped elastic net structure and estimated the mooring forces and mooring displacements. Yao et al. [18] proposed a hybrid volume approach to add the resistance force of the net cage into the flow field for coupling the fluid and net. Winthereig-Rasmussen et al.

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