



## Application of risk informed safety margin characterization to extended power uprate analysis



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### ABSTRACT

In this paper we present some initial results of the application of a risk-informed safety margin characterization (RISMC) approach to the analysis of the impact of an extended power uprate (EPU) on plant safety for selected transient and accident sequences. These initial applications were conducted to demonstrate the feasibility and practicality of using the RISMC approach to analyze the safety impact of EPUs at both a pressurized water reactor (PWR) and a boiling water reactor (BWR). For the PWR application, the analysis focused on the loss of main feedwater (LOMF) event with failure of auxiliary feedwater (AFW) where feed and bleed (F&B) cooling is required to prevent core damage. For the BWR case study, station blackout (SBO) sequences leading to core damage were analyzed. A consistent and repeatable process was developed and applied to identify those key parameters that would be analyzed. Distributions were constructed to represent the uncertainties associated with each of the key parameters. These distributions were sampled using a Latin Hypercube Sampling (LHS) technique to generate sets of sample cases that were used in the physics simulation runs using the MAAP4 code. Simulation results were evaluated to determine the changes to safety margins which would occur due to the uprated power conditions; the results obtained were then compared to those for the current nominal full power. The results obtained indicate, as expected, that safety margins may be reduced with increases in plant power level. However, for most power uprate levels, these safety margin reductions were found to be small. A limited study of margin recovery strategies was performed for the PWR case that indicated that minor to moderate changes in plant operation or design could be used to recover the safety margin reduction that would occur from the power uprate.

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### 1. Safety margin characterization framework

As described in earlier EPRI sponsored studies [1–5], the original design and licensing of commercial nuclear power plants (NPPs) ensured adequate safety margins by performing conservative engineering analyses and applying conservative judgment to specify appropriate safety limits for critical plant parameters. Maintenance of these safety margins has served as a foundational principle of plant operation and regulation since the advent of commercial nuclear power. However, as NPP lifetimes are extended beyond the initial approved license duration, and operational enhancements (such as EPUs) are made to achieve enhanced economic performance, there has developed a critical need to develop and apply an approach to evaluate and manage safety margins that is both technically justifiable and economical to implement. Additionally, since the accident at the Fukushima

Dai-ichi plant, a renewed focus on NPP safety analysis throughout the world is likely to increase the need to more systematically and comprehensively evaluate the impact of plant long-term operation (LTO) decisions on safety margins. These factors increase the need for a methodology that can be economically applied by licensees and can generate results that can be readily reviewed by regulatory personnel.

To address this need, ongoing research has been performed to develop and demonstrate risk-informed approaches to evaluate and characterize NPP safety margins. The basic framework is represented conceptually by the relationship

$$P(C > L)$$

which depicts the evaluation of a parameter (represented by a load  $L$ ) versus an acceptance guideline (represented by a capacity  $C$ ). Stated a different way, one is concerned with determining what is the probability that the load experienced during a particular analyzed event does not exceed the capacity to handle it? Although, in practice, this assessment has generally been simplified to the

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### Acronyms

AAC	alternate AC	LERF	large early release frequency
AC	alternating current	LHS	Latin hypercube sampling
AFW	auxiliary feedwater	LOMFW	loss of main feedwater
AGR	advanced gas reactor	LOOP	loss of offsite power
ALARA	as low as reasonably achievable	LR	large release
BWR	boiling water reactor	LTO	long-term operation
CCDP	conditional core damage probability	LWR	light water reactor
CCP	centrifugal charging pump	MAAP	modular accident analysis program
CD	core damage	NPP	nuclear power plant
CDF	core damage frequency	PCPL	primary containment pressure limit
CST	condensate storage tank	PCT	peak cladding temperature
ECCS	emergency core cooling system	PI	plant impact
EDG	emergency diesel generator	PORV	power operated relief valve
EF	error factor	PRA	probabilistic risk assessment
EPRI	Electric Power Research Institute	PTS	pressurized thermal shock
EPU	extended power uprate	PWR	pressurized water reactor
ERG	emergency response guideline	RCIC	reactor core isolation cooling
ESF	emergency safeguards feature	RCP	reactor coolant pump
FOM	figure of merit	RISMIC	risk informed safety margin characterization
FV	Fussell–Vesely	RPV	reactor pressure vessel
F&B	feed and bleed cooling	SBO	station blackout
HCTL	heat capacity temperature limit	SDP	significance determination process
HEP	human error probability	SG	steam generator
HPCI	high pressure coolant injection	SORV	stuck-open safety relief valve
HPI	high pressure injection	SSC	structures, systems and components
HPSW	high pressure service water	TAF	top of active fuel
LER	licensee event report	T–H	thermal–hydraulic
		UQ	uncertainty quantification
		US	United States

comparison of point estimate values, in reality these parameters are more accurately represented as distributions that account for the uncertainties associated with prediction of both the load and capacity. Fig. 1 conceptually illustrates the relationship between a calculated load (e.g., temperature, pressure, etc.) distribution and the capacity distribution for a structure, system or component (SSC). In this paradigm the concept of “margin” is transformed from a simple “distance” between the point estimates of the load and capacity to that of a probability that the load experienced will exceed the installed capacity to handle it. In this figure we also indicate how various aspects of NPP LTO could impact these margins over time by shifting or modifying the underlying load/capacity distributions. Note that a more complete discussion of safety margins, the potential impact of extended NPP operation on them, and prior foundational research on the RISMIC approach is discussed in detail in previous EPRI research [1].

In the research described in [2], the approach to characterizing the safety margins was specified as follows:

- “Load” assessment: Utilize an applicable systems code (which for the purposes of the demonstrations described in this paper was the MAAP4 code) to parametrically investigate the input parameters and their influence on one or more key outputs (e.g., peak core temperature, fraction of core with peak cladding temperature greater than some defined limit, etc.). To support these analyses, the bases for sensitive input parameter values were reviewed and an applicable distribution for each representative parameter was developed.
- “Capacity” assessment: Select key output parameters to be investigated. Review the technical bases for parameter acceptance guidelines and assign a distribution to the “capacity” limits.

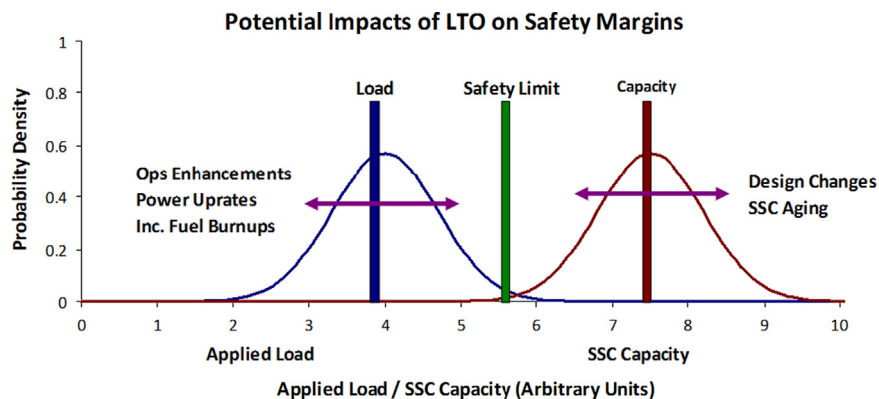


Fig. 1. Probability that SSC capacity exceeds load –  $P(C > L)$  – and potential impact of NPP LTO on safety margins [5].

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