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Convective heat transfer flow of nanofluid in a porous medium over wavy surface

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1. Introduction

Porous medium is characterized as a matrix containing pores. The structure of matrix is usually a solid and pores occupied by fluid. Network of pore and the solid matrix are continuous. Mostly, the properties of the medium like permeability, heat capacitance and thermal conductivity are sometime depended on solid matrix, media porosity and pores structure [1–3].

In industry, some processes are qualitatively influenced with deed of heat transfer enhancement. There are numerous ways to advance the efficiency in heat transfer. To improve convection heat transfer, one method is to use a medium which contains of solid matrix with an interconnected void called porous [4]. Transport and permeable media are becoming charming in design and analysis of heat exchanger and heat transfer devices. When the fluid moves through porous media, it contacts its wide area and heat transfer rate is enhanced in fluid due to tortuous shape of media. In addition, porous media is used to cooled or heated the fluids and to improve the thermal conductivity of fluids. Alkam and Al-Nimr [5] introduced a technique to improved convection heat transfer between fluid and tube walls. They used permeable

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ABSTRACT

In this letter, water base nanofluid flow over wavy surface in a porous medium of spherical packing beds is investigated. The copper oxides particles are taken into account. These properties are rehabilitated when fluid interacts with porous walls. For porous medium, Dupuit–Forchheimer model; an extension of Darcy's law model is utilized. The natures of velocity and temperature profiles of nanofluid are discussed graphically whereas the values of convection heat transfer coefficient in the presence of different nanoparticles concentrations in porous medium is presented in tabular form. The obtained results illustrate that convection heat transfer is improved by nanoparticles concentration but reduces when fluid attract to pores structured medium. On the other hand, when particles are added in fluid, convection heat transfer rate is improved but flow velocity is declined.

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substrates at both inner sides of wall of tubes and noted that coefficient of convective heat transfer is increase 50% in permeable medium as compare to without permeable medium. In another study [6], the flow and heat transfer characteristics of air in permeable media are investigated numerically and experimentally. Both experimental and numerical results illustrate that the convection heat transfer is improved significantly due high thermal conduction of solid metric in porous media. Ozgumus and Mobedi [7] investigated the Newtonian fluid flow in porous media which built by inline array of rectangular rods and calculated the influence of pore to throat size ratio on heat transfer coefficient. Their results show the enhancement in values of Nusselt number due the low pore to throat size ratios because the flow is entered the gaps deeply and walls of solid rectangular rods bands contribute on the heat transfer. Lin et al. [8] studied the effects of different pore size in bidisperse wick on heat transfer performance. Their results showed that the porosity and the permeability is not only factors in performance of heat transfer, but pore size distribution has great influence. Sumirat et al. [9] are discussed the properties of porosity on the thermal conductivity for nanoporous materials and give a way to design with higher or lower thermal conductivity to further used in heat exchanger or heat transfer applications.

Nanofluid is an important chemical fluid that is used in industries due to high heat transfer rates. Nanofluid show amazing thermo-physical properties that are not existed in the convective

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rs A ••• (••••) •••- ••• In Eq. (2), K is the permeability and c is Forchheimer coefficient which determined as

$$K = \frac{d^2 \varepsilon^3}{150(1-\varepsilon)^2},\tag{5}$$

$$c = \frac{1.75(1-\varepsilon)}{d\varepsilon^3},\tag{6}$$

where *d* is the particle diameter. The parameter ε shows the porosity of a packed-sphere bed.

Let us introduce the following non-dimensional variables

$$\bar{x} = \frac{x}{L}, \qquad \bar{y} = \frac{y}{L}Gr^{1/4}, \qquad \bar{u} = \frac{u}{u_o},$$
$$\bar{v} = \frac{Gr^{1/4}v}{U_o}, \qquad \bar{T} = \frac{T - T_\infty}{T_w - T_\infty}, \qquad Gr = \left(\frac{u_oL}{v_f}\right)^2,$$
(7)

where $u_o = [g\beta_f L(T_w - T_\infty)]^{1/2}$.

Substituting Eq. (7) in the Eqs. (1) to (4) and get the dimensionless forms of governing equations as follows

$$\frac{\partial \bar{u}}{\partial \bar{x}} + \frac{\partial \bar{v}}{\partial \bar{y}} = 0 \tag{8}$$

$$\frac{\mu_{nf}}{\mu_f} \frac{1}{\Lambda} \bar{u} + \frac{\rho_{nf}}{\rho_f} C \bar{u}^2 = \frac{1}{\varepsilon} \frac{\mu_{nf}}{\mu_f} \frac{\partial^2 \bar{u}}{\partial \bar{y}^2} + \frac{(\rho\beta)_{nf}}{(\rho\beta)_f} \overline{T},\tag{9}$$

$$\frac{(\rho C_p)_{nf}}{(\rho C_p)_f} \Pr\left(\bar{u}\frac{\partial \overline{T}}{\partial \bar{x}} + \bar{v}\frac{\partial \overline{T}}{\partial \bar{y}}\right) = \frac{k_{nf}}{k_f}\frac{\partial^2 \overline{T}}{\partial \bar{y}^2},\tag{10}$$

subject to boundary conditions

$$\bar{u} = \bar{v} = 0, \ \bar{T} = 1 \quad \text{at } \bar{y} = \sigma(L\bar{x}) \\ \bar{u} = 0, \ \bar{T} = 0 \quad \text{at } \bar{y} \to \infty$$
 (11)

In above $\bigwedge = KGr^{\frac{1}{2}}/L^2$ is dimensionless permeability parameter whereas C = cL is dimensionless Forchheimer coefficient.

Further, using the stream function formulation

$$\psi = \bar{x}f(Y), \quad \overline{T} = \bar{x}\theta(Y), \quad Y = \bar{y} - \sigma(L\bar{x}) \\ \bar{u} = \frac{\partial\psi}{\partial\bar{y}}, \quad \bar{v} = -\frac{\partial\psi}{\partial\bar{x}}$$
(12)

The resulting Eqs. (9)-(11) become

$$\frac{\mu_{nf}}{\mu_f} \frac{1}{\Lambda} f' + \frac{\rho_{nf}}{\rho_f} C^* f'^2 = \frac{1}{\varepsilon} \frac{\mu_{nf}}{\mu_f} f''' + \frac{(\rho\beta)_{nf}}{(\rho\beta)_f} \theta,$$
(13)

$$\frac{k_{nf_{eff}}}{k_f}\theta'' + \frac{(\rho C_p)_{nf_{eff}}}{(\rho C_p)_f} \Pr(f'\theta - f\theta') = 0,$$
(14)

with boundaries conditions

$$\begin{cases} f = 0, f' = 0, \theta = 1 & \text{at } \eta \to 0 \\ f' = 0, \theta = 0 & \text{at } \eta \to \infty \end{cases}$$

$$(15)$$

2.2. Nanofluid modeling

When nanoparticles are dispersed in base fluid, thermo-physical properties of fluids are improved which play important role in heat transfer, to minimize irreversible processes and other applications. So far, most studies on thermal properties of nanofluid have focused on viscosity and thermal conductivity. However, heat transfer characteristics also depend on other properties, such as specific heat, thermal expansion and density etc. In Eqs. (9) and (10), physical properties such as thermal expansion coefficient β_{nf} , density ρ_{nf} and viscosity μ_{nf} for the nanofluid are given as,

ids, many researches associated with various nanofluid's applications have been investigated. Some of the applications contain; electronic cooling, car radiators, heat pipes, nuclear plant, coolant in welding and machining, heat exchanger, etc. Since for the last one decade, studies on the nanofluid have been augmented rapidly [10–13]. Choi et al. [14] prepared oil base Al₂O₃/AIN-nanofluid. By this nanofluid, they found 8% improvement of thermal conduction and overall the value of heat transfer coefficient is improvement 20% at 0.5% nanoparticles volume fraction. The performance in heat transfer in water base hybrid nanofluid in tubular heat exchanger is investigated experimentally by Madhesh and Kalaiselvam [15] through titania-copper nanomaterial. Their results illustrate up to 30.4% improvement in heat transfer coefficient at 0.7% concentrations of hybrid nano composite. A fully developed flow of water base (Cu-Al₂O₃)-nanofluid along convective heat transfer behavior in heated circular tube were examined by Suresh et al. [16]. The experimental results of this showed a 6.09% enhanced in Nusselt number via Al₂O₃ nanoparticles at 0.1% concentration when related to water. In another study, Suresh et al. [17] calculated the heat transfer behavior in turbulent flow of water base (Al₂O₃-Cu) nanofluid and found 8.02% enhancement in heat transfer rate as compared to water.

heat transfer fluids like water, oil etc. After discovery of nanoflu-

Recently, porous media with nanofluid is suited highly due great potential for heat transfer enhancement. Many studies in literature [18–21] are exposed that the convective heat transfer is improved through porous medium as well as nanoparticles due to having high thermal conductivity. An opportunity is offered for engineers to develop highly effective and compact heat transfer equipment by porous media and nanofluid. Further investigations covering the aspect of said topic can be consulted through the studies [22–40].

Motivated to all above facts, nanofluid flow through porous medium over wavy surface is investigated in the present study. For porous medium, Dupuit–Forchheimer model is used which is extension of Darcy's law model. For nanofluid, consider water as base fluid and modify its physical properties by copper oxides particles. The velocity and temperature profiles as well as convection heat transfer coefficient is exam under various particle concentrations and different percentage of porosity medium.

2. Mathematical formulation

2.1. Flow modeling

Consider the non-Darcy flow of nanofluid over vertical wavy surface. The dimensional coordinates along and normal to surface are denoted by x and y respectively. The porous structure and fill fluid are in thermodynamic equilibrium and temperature of surface is considered greater than ambient fluid temperature. Under boundary layer and Boussinesq approximations, the governing equations are

$$\frac{\partial u}{\partial x} + \frac{\partial u}{\partial y} = 0,\tag{1}$$

$$\frac{\mu_{nf}}{K}u + \rho_{nf}cu^2 = \frac{\mu_{nf}}{\varepsilon}\frac{\partial^2 u}{\partial y^2} + g(\rho\beta)_{nf}(T - T_\infty), \qquad (2)$$

$$(\rho C_p)_{nf_{eff}} \left(u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} \right) = k_{nf_{eff}} \frac{\partial^2 T}{\partial y^2}.$$
 (3)

Subject to

$$u = v = 0, T = T_w \text{ at } y = \sigma(x) = Sin(x) u = 0, T = T_\infty \text{ as } y \to \infty$$

$$(4)$$

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