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# Assessment of evaporation equilibrium and stability concerning an acoustically excited drop in combustion products

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#### ABSTRACT

The evaporation of drops in a sound field has been the subject of numerous studies aimed at determining its role in combustion instability. The models generally assume local equilibrium evaporation at the interface. We determine here the conditions of validity of this assumption, without calling into question other a priori assumptions of the classical model, in particular spherically symmetric quasi-steady evolution in the gas phase and liquid phase thermal unsteadiness with pure heat conduction.

Another possible phenomenon concerns the differential recoil of the vapor. In the case of rapid evaporation, a pressure difference appears between both sides of the interface, even if the latter is plane. This pressure difference, usually neglected, is proportional to the square of speed and the resulting force is oriented toward the denser fluid, i.e. the liquid. A very fast evaporation may even cause local deformation, i.e. Hickman instability. The stability condition concerning this phenomenon has also been determined.

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#### 1. Introduction

The evaporation of drops in an acoustic field has been the subject of many studies aimed at determining its role in combustion instability. The models generally assume local evaporation equilibrium at the interface. We want to determine here the conditions of validity of this assumption, without questioning the other a priori assumptions of the classical model, in particular: spherical symmetry, quasi-stationary evolution in the gas phase and thermal unsteadiness of the liquid phase with pure heat conduction [1,2].

*The local evaporation equilibrium* is characterized by the equality of chemical potentials of the constituent of the drop in liquid and vapor phases,

$$\mu_{\rm FL} = \mu_{\rm FV}$$

(1)

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#### Nomenclature

a, b, c	constant coefficients	<i>x</i> , <i>y</i> , <i>z</i>	Cartesian coordinates
А, В	thermodynamic coefficients in the transfer	Ζ	transfer function of the fed oscillating droplet
	function	$\alpha, \alpha_{\rm v}, \alpha_{\rm c}$	evaporation-condensation, vaporization, con-
$B_{\rm M}, B_{\rm T}$	Spalding parameters for mass and temperature		densation coefficients respectively
C <sub>p</sub>	specific heat at constant pressure	$\bar{\alpha}$	coefficient of the transfer function of the fed
Ċ	combustion chamber level		oscillating droplet
d	droplet diameter	$-\beta_{I}$	thermal gradient in a liquid boundary layer
Da	Damköhler parameter	δ	thickness of a boundary layer ( $\delta$ for the vapor
$E(u, \theta)$	function $E(u, \theta) = 1 - (1 + i)\sqrt{3u/2\theta} \operatorname{coth}[(1 + i)\sqrt{3u/2\theta}]$	0	side. $\delta_{\rm L}$ for the liquid one)
	i) $\sqrt{3u/2\theta}$	λ	heat conductivity
g	thermodynamic potential per unit mass, grav-	n(x v t)	function describing a disturbed surface $z =$
•	itational acceleration	.,(, , , , , , , ,	n(x + y) the reference value being zero
G	gas phase	к	heat diffusivity
h	liquid height		dynamic viscosity: thermodynamic potential
Н	container height	μ	ner mole $\mu = M\sigma$
Hi	Hickman number		chemical potential of species $i$
k	heat conductivity	$\mu_j$	quantity equal to: $(1 \pm i) \sqrt{3u/2\theta}$
1	latent heat per unit mass	⊥ ⊒	qualitity equal to: $(1+1)\sqrt{3u/20}$
L	liquid phase; phenomenological coefficient for	П	tensor of viscous pressures
	near-equilibrium evaporation-condensation	$\theta_{-}$	ratio $\tau_{v}/\tau_{T}$
М	mass	$\Theta$	reduced temperature
$\mathcal{M}$	molar mass	$ ho,  ho_{L}$	gas and liquid densities
<i>m</i>	unit mass flow rate	σ	surface tension
М	mass flow rate for an evaporating droplet	τ	characteristic time; $ au_{vap}$ for evaporation–
Ν	response factor $N = \bar{\alpha} \Re(Z)$		condensation; $ au_{ m mec}$ mechanical time
Ň	unit normal at a point of an interface; quantity	$ au_{ m excit}$	period of an oscillating disturbance
	$\vec{\nabla} \cdot \vec{N}$ being the average normal curvature	$ au_{\mathrm{T}}, ilde{ au}_{\mathrm{T}}$	characteristic times for heat diffusion respec-
D	thermodynamic pressure		tively in the gas, $\tau_{\rm T} = \delta^2 / \kappa$ and in the liquid,
p <sub>sat</sub>	saturation pressure		$\tilde{\tau}_{\mathrm{T}} = \bar{r}_{\mathrm{S}}^2 / \kappa_{\mathrm{L}}$
ат ат	coefficient equal to $\tau_{\rm T}/6\pi \tilde{\tau}_{\rm T}$	$\bar{ au}_{v}$	mean residence time of the injected liquid for
r	gas constant per unit mass $r = R/M$		a fed drop; equal to the lifetime $\tau_{\text{life}}$ of the
r.	mean radius of the fed droplet		free droplet
Ŗ	universal gas constant	ω	pulsation of an oscillating wave
S	interface level: cross section area	ξ	reduced radius $\xi = r/\bar{r}_s$
T	temperature in K	ζT	reduced variable $\zeta_{\rm T} = \dot{M}c_{\rm p}/4\pi kr$
и	reduced pulsation: $u = 3\omega \bar{\tau}_{v}$	*	reference conditions
V	speed	_	the liquid side of the interface
v	fluid velocity	+	the vapor side of the interface
ŵ	interfacial velocity		tangentially to the interface
We	Weber number: $We = \rho (V_C - V_I)^2 / \sigma$	1	normally to the interface

In the case of *local evaporation non-equilibrium*, the equality of chemical potentials is no more guaranteed and the mass flow rate of vaporization is a function of their difference. According to Bond and Struchtrup [3], in the case of a pure substance, the rate of evaporation can be written:

$$\dot{m} = \left(\frac{\mathcal{M}}{2\pi R}\right)^{1/2} \left(\alpha_{\rm v} \frac{p_{\rm sat}}{(T_{\rm S})^{1/2}} - \alpha_{\rm c} \frac{p^+}{(T^+)^{1/2}}\right) \tag{2}$$

with two different coefficients  $\alpha_v, \alpha_c$ , respectively for evaporation and condensation,  $\mathcal{M}$  the molar mass, R the universal gas constant,  $p_{sat}$  the saturation vapor pressure at the temperature  $T^- = T_S$  of the liquid surface,  $T^+, p^+$  corresponding to the gas. Coefficient values  $\alpha_v, \alpha_c$  become equal when one tends towards equilibrium:  $\alpha_v = \alpha_c = \alpha$ .

Another phenomenon can occur during very fast evaporation, changing the shape of the liquid–vapor interface. It is called the *vapor recoil* (see Appendix A.1). It can be explained by the momentum balance at the interface and results in a force acting towards the densest fluid, i.e. the liquid.

The case of vacuum evaporation, which results in surface deformation, has been particularly studied by Palmer [4], who found the stability limit of the phenomenon. This is the *Hickman instability* [5] (see Appendix A.2).

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