



# Identification of novel dual-scale Al<sub>3</sub>BC particles in Al based composites



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## ABSTRACT

In this work, the Al<sub>3</sub>BC/Al (Al–3Cu) composites have been firstly in-situ fabricated by liquid–solid reaction method. The microstructures of the samples were investigated by X-ray diffraction (XRD), scanning electron microscope (SEM) and transmission electron microscope (TEM). Two typical sized Al<sub>3</sub>BC particles of 100–300 nm and 5–20 nm have been in-situ fabricated, and the particles show the uniform distribution. Mechanical property tests reveal the remarkable coordinated enhancement effects of dual-scale Al<sub>3</sub>BC particles. The hardness, tensile strength and abrasion resistance of 26% Al<sub>3</sub>BC/Al–3Cu composite are improved by 106.3%, 143.5% and 27.3% respectively, compared with the unreinforced alloy. The synthesis mechanisms of Al<sub>3</sub>BC are also discussed and two different mechanisms are proposed to explain the formation of the dual-scale particles.

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## 1. Introduction

Aluminum boron–carbide phases (such as Al<sub>3</sub>BC<sub>3</sub>, Al<sub>8</sub>B<sub>4</sub>C<sub>7</sub>, AlB<sub>2</sub>C<sub>4</sub>, etc.) in the Al–B–C system have become the topics of several current investigations since composites reinforced by them possess excellent properties such as high strength, high hardness and low density [1–3]. Besides the above compounds, Al<sub>3</sub>BC is another promising phase, which was firstly described as phase X by Halverson et al. in B<sub>4</sub>C/Al composites [4]. It is the main product of the interface reaction between B<sub>4</sub>C and Al in B<sub>4</sub>C/Al composites and has great influence on the mechanical properties of the composites [5–11]. By using X-ray investigations on the powder samples, Viala et al. [12] reported the crystal lattice of Al<sub>3</sub>BC which has a hexagonal unit cell with  $a = 3.491(2)$  Å and  $c = 11.541(4)$  Å. Later, Meyer and Hillebrecht [13] synthesized the pure Al<sub>3</sub>BC and defined its crystal structure as a closest packing of Al atoms (sequence ABACBC) with alternating layers of edge-sharing BA<sub>6</sub> octahedra and trigonal bipyramids CA<sub>5</sub>, linked by common corners. After that, Solozhenko et al. [14] reported the thermal stability of Al<sub>3</sub>BC and indicated that even under a high pressure of 1.6–4.8 GPa, the phase remains stable up to 1700 K, implying its high stability. The calculated bulk modulus (152 GPa), shear modulus (140 GPa) and the Young's modulus (326 GPa) of Al<sub>3</sub>BC were given in Ref. [15].

However, the current applications of Al<sub>3</sub>BC are rarely reported due to the fabrication difficulties of Al<sub>3</sub>BC. Ma et al. [16] suggested that Al<sub>3</sub>BC was an effective refiner of magnesium alloys. The Al–1B–0.6C master alloy which contains micron-scale Al<sub>3</sub>BC particles with size of 2–8 μm can effectively reduce the grain size of AZ63 alloy from 710 μm to 70 μm. In addition, Al<sub>3</sub>BC is used as the raw material to

manufacture Al–5Ti–0.8B–0.2C master alloy which acts as an effective refiner for aluminum alloys and the transformation process from Al<sub>3</sub>BC phase to doped TiB<sub>2</sub> or TiC particles in Al–Ti melts was reported in reference [17]. In our work, a new application of Al<sub>3</sub>BC as reinforcement for aluminum composites has been proposed. With low density, high hardness, excellent thermal stability and remarkable stiffness, Al<sub>3</sub>BC is regarded as a competitive candidate as the strengthening phase for aluminum composites.

Even if many reinforcements such as SiC, Al<sub>2</sub>O<sub>3</sub>, TiB<sub>2</sub>, and TiC have been widely investigated at present [18–21], there remain unsolved problems such as the segregation phenomenon resulting from the distinction between reinforcements and the matrix alloys and the aggregation tendency of the reinforcement like TiB<sub>2</sub>. Compared with them, Al<sub>3</sub>BC has its own advantages. On one hand, it has much lower density (2.83 g/cm<sup>3</sup>) than those of Al<sub>2</sub>O<sub>3</sub> (3.98 g/cm<sup>3</sup>) and TiB<sub>2</sub> (4.50 g/cm<sup>3</sup>) etc., which is more likely to achieve the demand of lightweight. On the other hand, the density of Al<sub>3</sub>BC is very close to that of the Al matrix (2.70 g/cm<sup>3</sup>); as a result, the sedimentation behavior in the Al melt during the process is relatively weak, which is beneficial to getting a homogenous distribution of the reinforcement. In addition, Al<sub>3</sub>BC has high elastic modulus and excellent thermal stability as well as fine size, which also makes it appropriate to act as the strengthening phase in aluminum alloys.

The mass fabrication and morphology control of Al<sub>3</sub>BC particles have become very essential for real applications, however, only few papers are documented. Takeshi et al. [22] fabricated Al<sub>3</sub>BC using aluminum powders, amorphous boron powders and graphite powders as raw materials through the self-propagating high-temperature synthesis (SHS) method. According to Kubota's work [23], Al<sub>3</sub>BC can also be synthesized by solid-state reactions occurring during heat treatments after mechanical milling (MM) of pure aluminum with 15 or 50 at.% MgB<sub>2</sub> powder

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mixtures in the presence of the process control agent (PCA). However, all these papers reported few on the microstructure and morphology control of  $\text{Al}_3\text{BC}$  particles.

In this work, the novel  $\text{Al}_3\text{BC}$  reinforced Al or Al–Cu based composites have been in-situ synthesized through a liquid–solid reaction method for the first time and the  $\text{Al}_3\text{BC}$  particles fabricated in this way possess dual-scale sizes and uniform distribution in the matrix. The microstructures, mechanical properties and synthesis mechanisms have also been investigated in this work.

## 2. Experimental details

The raw materials used in this work contained commercial Al (99.7%, all compositions quoted in this work are in wt.% unless otherwise stated), graphite powders (99.0%, 5–10  $\mu\text{m}$ ) as well as boron plasmid. The  $\text{Al}_3\text{BC}/\text{Al}$  (or Al–3Cu) composites were in-situ fabricated through a liquid–solid reaction method at 750 °C and then were extruded at 500 °C to decrease the porosity.

X-ray diffraction technology was used to identify the phases contained in the composites and the microstructure of the alloys were characterized utilizing field emission scanning electron microscope (FESEM, model SU-70, Japan), equipped with an energy dispersive X-ray spectroscopy (EDS) detector. Transmission electron microscope (TEM, JEM-2100) was also used to identify the morphology and structure of the nanoscale  $\text{Al}_3\text{BC}$  particles.

To verify the strengthening effects of  $\text{Al}_3\text{BC}$  on the matrix, the hardness, tensile properties as well as the abrasion tests on Al–3Cu matrix composites with  $\text{Al}_3\text{BC}$  concentration of 13% and 26% (all the  $\text{Al}_3\text{BC}$  concentration quoted in this work are nominal unless otherwise stated) after T6 heat treatment (solution treatment at 515 °C for 15 h and aging at 165 °C for 15 h) were carried out.

The hardness test bars were machined to the cube type specimens (30 mm in length, 20 mm in width and 20 mm in height) and then tested on a HBS-3000 digital Brinell hardness tester according to the ASTM E10–14 standard. The diameter of the indenter is 5 mm, and the force is 2452 N (250 kgf) with dwell time of 60 s. Each value was an average of at least four separate measurements taken at random places of the specimens. The tensile test was conducted on ‘dog-bone’ type specimens

shown in Fig. 1a using a CMT700 universal material test machine at ambient temperature according to the ASTM E08 standard. In each case, four specimens were tested and the average values were reported. The wear-resistance test was performed on a MM200 abrasion tester according to ASTM G77 standard, and the schematic diagrams of abrasion test are shown in Fig. 1b. The wear specimens with 10 mm  $\times$  10 mm in cross-section and 45 mm in length were used with load of 120 N and rotating speed of 400 r/min. The mass loss of the specimens was measured every 10 min to calculate the mass loss–time curves. The wear rate defined as the abrasion loss per unit time was calculated to quantitatively verify the strengthening effects of  $\text{Al}_3\text{BC}$  on the wear-resistance. Friction coefficients under a series of load pressure were also measured in this work.

## 3. Experimental results

### 3.1. In-situ synthesised $\text{Al}_3\text{BC}$ in the Al matrix

To investigate the in-situ synthesis behaviors and the microstructures of  $\text{Al}_3\text{BC}$  particles in the aluminum melt,  $\text{Al}_3\text{BC}/\text{Al}$  composites which contain about 26%  $\text{Al}_3\text{BC}$  particles were fabricated and the XRD pattern and microstructures of the samples are shown in Fig. 2. Based on the XRD pattern in Fig. 2a, besides the Al matrix, only the  $\text{Al}_3\text{BC}$  phase was detected in the sample. Fig. 2b presents the typical microstructure of the sample and the small-sized white phases distributing uniformly in the matrix are detected to be  $\text{Al}_3\text{BC}$  particles with the reference of the XRD and EDS results. High magnification images in Fig. 2c–d reveal that  $\text{Al}_3\text{BC}$  particles with tetradecahedron morphology have size ranging from 100 to 300 nm.

Since the  $\text{Al}_3\text{BC}$  particles are too small to be characterized in detail by SEM, the TEM analysis has been carried out to identify their morphology and structure, as shown in Fig. 3. Besides the  $\text{Al}_3\text{BC}$  with size ranging from 100 nm to 300 nm as mentioned in Fig. 2, more spherical particles with size ranging from 5 nm to 20 nm appear in the Al matrix as shown in Fig. 3a, which are also identified to be  $\text{Al}_3\text{BC}$  by HRTEM analysis in Fig. 3b and the result of FFT process in Fig. 3c. The interplanar spacing of the particle in Fig. 3b is calculated to be 1.76 Å, which approximately equals to that of the {110} plane of  $\text{Al}_3\text{BC}$ . Fig. 3d displays the fast Fourier

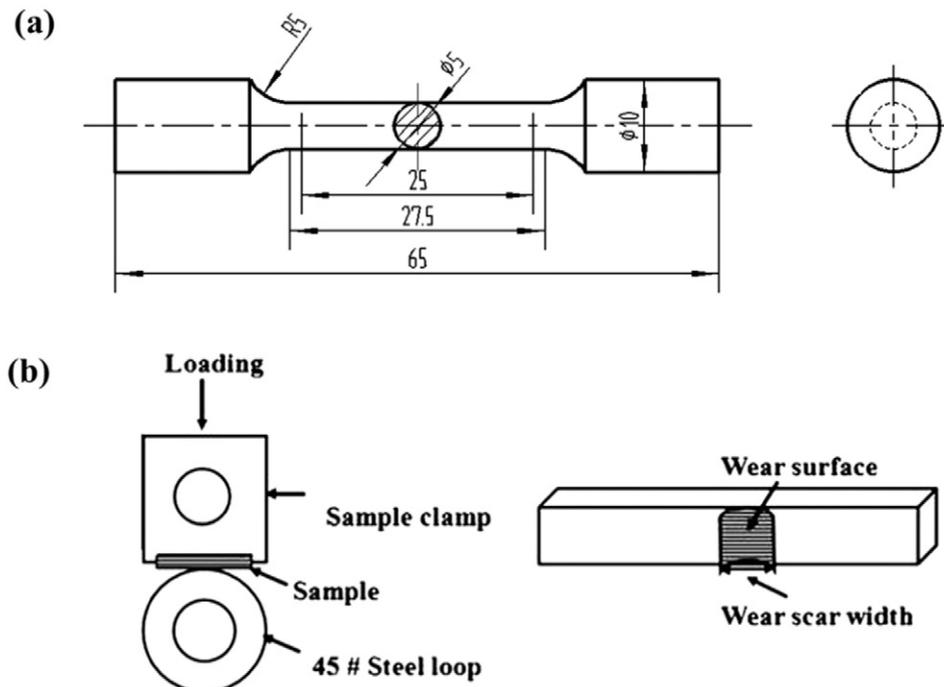


Fig. 1. Schematic diagrams of the tensile and abrasion test specimens: (a) tensile test specimen and (b) abrasion test specimen.

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