European Journal of Pharmaceutics and Biopharmaceutics xxx (2015) xxx-xxx

Contents lists available at ScienceDirect



European Journal of Pharmaceutics and Biopharmaceutics

journal homepage: www.elsevier.com/locate/ejpb

## 2 Research Paper

## Accuracy of micro powder dosing via a vibratory sieve-chute system

M.O. Besenhard <sup>a,b,1</sup>, E. Faulhammer <sup>a,b,1</sup>, S. Fathollahi <sup>a</sup>, G. Reif <sup>b</sup>, V. Calzolari <sup>c</sup>, S. Biserni <sup>c</sup>, A. Ferrari <sup>c</sup>, S.M. Lawrence <sup>d</sup>, M. Llusa <sup>a</sup>, J.G. Khinast <sup>a,b,\*</sup>

<sup>a</sup> Research Center Pharmaceutical Engineering (RCPE) GmbH, 8010 Graz, Austria

<sup>b</sup> Graz University of Technology, Institute of Process and Particle Engineering, 8010 Graz, Austria

<sup>c</sup> MG2, Via del Savena 18, I-40065 Pian di Macina di Pianoro, Bologna, Italy
<sup>d</sup> ClaxoSmithKline (CSK), New Frontiers Science Park, Harlow, Essex CM19 5AW, UK

## ARTICLE INFO

36

5 4

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13 14

Article history:
Received 24 February 2015

19 Revised 23 April 2015

- 20 Accepted in revised form 29 April 2015
- 21 Available online xxxx
- 22 Keywords:
- 22 Keywords:23 Micro dosin
- 23 Micro dosing24 Micro feeding
- 25 Capsule filling
- 26 Vibratory sieve
- 27 Online scale
- 28 Lactose

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#### 44 45 **1. Introduction**

Precise dosing of small powder quantities is required in many 46 industrial operations and is a focus of intense research. In recent 47 years, granular 3D printing (e.g., direct, selective or laser sintering 48 49 [1,2]) became state-of-the-art, introducing a multitude of applica-50 tions ranging from rapid prototyping to tissue engineering [3–8]. 51 The incorporation of functional gradients via multiple components 52 requires low dosing of powders to accomplish high resolutions [9]. 53 Hence, many recent developments in low dosing address 54 free-forming methods (such as 3D printing).

In pharmaceutical development and manufacturing, precise 55 powder filling remains a challenge [10,11]. Regulatory require-56 57 ments impose a high dose uniformity, especially when the therapeutic window is narrow [12], which is – for example – the case 58 for dry powder inhalers (DPI) [13-15] that deliver small quantities 59 of highly-potent active pharmaceutical ingredients (APIs). A cur-60 rent trend in oral solid dosage forms as well as in inhalation appli-61 cation is dosing small quantities of a pure API into a capsule, 62 63 effectively avoiding fillers, binders, lubricants, flavoring agents,

<sup>1</sup> First authorship equally shared.

http://dx.doi.org/10.1016/j.ejpb.2015.04.037 0939-6411/© 2015 Elsevier B.V. All rights reserved.

ABSTRACT

This paper describes a powder dosing system with a vibratory sieve mounted on a chute that doses particles into a capsule. Vertical vibration occurred with a broad range of frequencies and amplitudes. During dosing events, the fill weight was accurately recorded via a capacitance sensor, covering the capsules and making it possible to analyze filling characteristics, that is, the fill rates and their robustness. The range of frequencies and amplitudes was screened for settings that facilitated reasonable (no blocking, no spilling) fill rates for three lactose powders. The filling characteristics were studied within this operating space. The results reveal similar operating spaces for all investigated powders. The fill rate robustness varied distinctly in the operating space, which is of prime importance for selecting the settings for continuous feeding applications. In addition, we present accurate dosing studies utilizing the knowledge about the filling characteristics of each powder.

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and the associated efforts and risks in the formulation development. Furthermore, there is an increasing interest in continuous processing, which demands robust low-dose feeders for APIs [16–18].

Most dosing techniques used in capsule filling [15,19] involve volumetric filling principles, such as dosator nozzle systems [20–23], vacuum or pneumatic dosators [24–26] and tamp fillers [27,28]. All of them initially place powders into chambers of a fixed volume that define the final dosage. Since most volumetric techniques require powder beds, there is always some waste powder created [15]. Although volumetric dosing is generally faster, for precision dosing, other methods are preferred [5]. Nevertheless, low-dose filling (<10 mg) with nozzle dosator systems [29] and drum dosing [30] have been studied recently.

For accurate low-(or micro-) dosing, gravimetric techniques are better suited. Micro-dosing via vibrating capillaries or rods [31–33] (also in the ultrasonic regime [9,34,35]) is a promising low-dosing and feeding technique, which is currently investigated for solid-dosing applications. For example, it was reported that highly accurate low dosing (relative standard deviation of fill weight below 5%) can be performed via the "pepper-shaker" principle (MG2 Microdose, Capsugel Xcelodose®S or 3P Innovation Fill2weight) for capsule filling [36,37]. Furthermore, micro-feeding (<1 mg/s) has successfully been performed via auger methods [38,39] and vibratory channels [9,40,41] and vibrating spatulas [42].

<sup>\*</sup> Corresponding author at: Graz University of Technology, Institute of Process and Particle Engineering, 8010 Graz, Austria. Tel.: +43 (316) 873 30400; fax: +43 (0) 316 873 30402.

E-mail address: khinast@tugraz.at (J.G. Khinast).

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Nomen	clature	
		Symbols
Abbrevi	ations	C <sub>filled</sub> filled capsule
Α	amplitude	C <sub>empty</sub> empty capsule
API	active pharmaceutical ingredient	ε difference between target weight and fill weight
BD	bulk density	fw fill weight
CI	Carr index	<i>fw<sub>target</sub></i> target fill weight
DPI	dry powder inhaler	<i>k<sub>cal</sub></i> calibration factor of the capacitive scale
F	frequency	<i>K<sub>d</sub></i> DERIVATIVE constant of PID control
FFC	flow function	<i>K<sub>i</sub></i> integrative constant of PID control
PID	proportional integrative derivative	<i>K<sub>p</sub></i> proportional constant of PID control
PSD	particle size distribution	$\sigma_1$ consolidation stress
RSD	relative standard deviation	$\sigma_c$ unconfined yield strength
RH	relative humidity	<i>t<sub>i</sub> i</i> th time step
SV	sieved	$x_{10}$ , $x_{50}$ , $x_{90}$ 10%, 50% and 90% of the PSD reside below the particle
TD	tapped density	size x
	* * *	

90 This study is an in-depth analysis of a gravimetric micro-dosing system for fine powders in the milligram range based on the 91 "pepper-shaker" principle. Hard gelatin capsules were filled 92 93 directly via a sieve merged with a vibrating chute. The device 94 (MG2 Microdose) was equipped with a capacitive scale, making it possible to analyze the effect of process settings on the filling 95 characteristics. An operating space was created for three common 96 97 excipients in inhalation products (i.e., lactose powders [43,44]) and the results were analyzed to establish the optimal settings for con-98 99 tinuous micro-feeding. Furthermore, the limitations of the 100 low-dose accuracy were addressed by performing dosing experi-101 ments with a target weight of 2.5 mg.

#### 2. Materials and methods 102

#### 103 2.1. Materials

Three grades of inhalation-grade  $\alpha$ -lactose monohydrate (here-104 inafter referred to as lactose) excipients with different particle 105 106 sizes and supplied by different manufacturers (DFE Pharma, 107 Germany; Meggle, Germany) were used as received.

#### 2.2. Material characterization 108

Particle size, density and flow behavior were investigated and 109 each measurement was done in triplicate (n = 3). 110

#### 2.2.1. Particle size characterization 111

Particle size distribution was determined using laser light 112 113 diffraction technique (HELOS/KR, Sympatec GmbH, 114 Clausthal-Zellerfeld, Germany). A dry dispersing system 115 (Rodos = L, Sympatec) and a vibrating chute (Vibri, Sympatec) were 116 used for powder dispersion. A dispersion pressure of 2.5 bar was 117 applied. The typical sampling time was 30 s. Evaluation of the data was performed using the software Windox 5 (Sympatec). 118

#### 119 2.2.2. Bulk density and tapped density

The bulk (BD) and tapped densities (TD) were analyzed 120 (Pharmatest PT-TD200) via a standardized method described in 121 the United States Pharmacopeia (USP 2011, (616)). A certain mass 122 of powder was filled into the cylinder and the level was recorded. 123 124 The tapped density was attained after mechanically tapping the 125 powder sample. Carr's Compressibility Index (CI) is a 126 density-based index assessed out of TD and BD and indicates

(2015), http://dx.doi.org/10.1016/j.ejpb.2015.04.037

how a powder changes its density upon tapping. Large changes indicate poor flowability.

## 2.2.3. Powder flow measurements

The flow function (FFC) was measured using the FT4 Powder Rheometer (Freeman Technology, UK) adjusted with a 1 ml shear cell module at a maximum pressure of 3 kPa. FFC is the ratio of consolidation stress,  $\sigma_1$ , to unconfined yield strength,  $\sigma_c$ . A high FFC value indicates that the powder should flow well.

Respitose SV003 is a sieved carrier (for inhalation APIs) and 135 SV010 is a coarse sieved carrier. Both have a narrow particle size distribution (PSD). InhaLac 230 (Meggle, Germany) is a sieved car-137 rier with the lowest PSD of the investigated samples. The three carrier systems had similar values of bulk and tapped densities. An overview of the particle sizes and powder flow attributes of these materials is provided in Table 1 [29]. As can be seen Respitose 141 SV010 had a slightly better flowability than the other powders. All three powders were in a range of "close to good" flowability, with CI < 15 indicating good flowability and CI > 25 indicating poor 144 powder flow behavior. The FFC of the powders indicates good 145 flowability in all cases, with Respitose SV003 having the best value.

## 2.3. Process and equipment

## 2.3.1. Vibratory sieve chute system

We used the MG2 Microdose stand-alone unit, a dosing system with a vibratory sieve (oscillating vertically) mounted on top of a chute (2.5 cm) to guide the powder into the capsule. Fig. 1 shows the operating principle and parts of the set-up. The chute is tilted at a fixed angle of  $5^{\circ}$  and the sieve with 10 holes of 0.7 mm in diameter is fixed on its top. The powder was discharged from the sieve into the chute and the capsule body using gravity. Every capsule was loaded manually.

The fill weight during the dosing events was recorded via a 157 capacitance sensor, which had two parallel electrode plates 158 encompassing the capsule body. The electrical field and the capac-159 itance varied depending on the powder quantity in the capsule. In 160 order to correlate the capacity *C<sub>filled</sub>* (relative to the capacity of an 161 empty capsule  $C_{empty}$ ) with the capsule fill weight fw, the sensor 162 had to be calibrated (Eq. (1)). The calibration factor  $k_{cal}$  was deter-163 mined based on the weight measurements performed on a SI-234A 164 (Denver Instruments) scale. The calibration was executed for a 165 given powder prior to the experimental studies. The accuracy of 166 the capacitive scale was best (<0.1 mg deviation from laboratory 167 scale) if *fw* was in the range of the fill weight used for calibration. 168

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