



# Transmission performance of OSSB-RoF system using MZM electro-optical external modulator

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## ABSTRACT

Both the EAM and the MZM, the commonly used electro-optical external modulators in RoF systems, have pointed on their transfer function curve at which link performance is optimized. In discussing the difficulty of maintaining the optimum modulator bias point, we prefer MZM because unlike EAM, it has a predictable transfer function shape. In this paper, the simulative investigation is analyzed and discussed to study the impact of extinction ratio with low chirp of single- and dual-electrode Mach–Zehnder (SEMZM and DEMZM) external modulators over RF power degradation introduced in Radio-over-Fiber (RoF) systems due to fiber dispersion, which is one of the limiting factors to RoF link. Our simulative results show that longer transmission distance spanned between a receiver and transmitter with minimum RF power degradation can be achieved by using low extinction ratio and chirp of MZM modulators. Further, it is also observed that a dual-electrode MZM with low extinction ratio and chirp enables the transmission of RF signal not only with minimal dispersion but also with maximal second-order harmonic (HD2) reduction.

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## 1. Introduction

For realization of future high performance integrated networks, broadband distribution and access networks and to meet the increasing demand of multimedia services with a guaranteed quality of service, RoF technology comes out as the most promising technology. RoF technology combines the capacity of optical networks with the flexibility and mobility of wireless networks. Reduction in complexity at the antenna site, reduction in installation cost of access networks, possibility of dynamically allocation of radio carriers to different antenna sites, transparency and scalability are the few advantages of Radio-over-Fiber (RoF) technology. The applications of RoF technology include cellular networks, satellite communication, Multipoint Video Distribution Services (MVDS), Mobile Broadband System (MBS) and Wireless LANs over optical networks [1]. RoF technology involves the use of optical components and techniques to allocate RF signals from the control stations (CS) to the base stations (BS). Thus, RoF makes it possible to centralize the RF signal processing function in one shared location (CS) with use of single mode optical fiber that has a very low signal loss to distribute the RF signals to the BSs [2].

The micro and pico-cellular architectures are installed with low power radio access points (RAPs) to increase the frequency reuse and capacity of a wireless network to provide wireless access. The best way to connect these RAPs to CS unit is RoF technology. Further, RoF technology allows a fiber-fed distributed antenna network to be implemented that provides several advantages such as low RF power remote antenna units, frequency reuse, better coverage, high capacity, high quality signal as well as low fiber attenuation. Further, with RoF technology, the antenna need not be within the control area but can be sited a lot of kilometers away for the purpose of improved satellite visibility or reduction in interference from other terrestrial communication systems.

Several methods have been reported for the generation of modulated RF optical carriers in fiber-wireless systems. However, the simplest technique for the optical generation and distribution of the RF signal modulated with data is an intensity modulation scheme via direct or external modulation of a laser in which the RF signals are either externally or directly modulated onto the optical carrier. But, the frequency chirping due to the direct modulation of a semiconductor laser limits the transmission bandwidth of RoF system. An external modulation technique is an alternative candidate in order to eliminate this problem. Currently, two types of external modulators are commercially available and can be considered for use in high-bit-rate digital or high-performance microwave fiber-optic links. Because of having a predictable transfer function shape,

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we prefer MZM over EAM external modulators in RoF systems. By controlling the amplitude of the drive signals applied to two electrodes of Dual Electrode Mach–Zehnder (DEMZM) modulators, both the chirp and the extinction ratio of the signal can be precisely adjusted to extend transmission distance without dispersion compensation [3,4]. Dual-drive MZ modulators are also important for high spectral efficiency dense wavelength-division-multiplexed (DWDM) systems since the minimum mean-square bandwidth are achieved when the transmitted signal contains no chirp [5]. However, it has been reported through computer simulation that an MZ modulator with a finite dc extinction ratio will always be accompanied by residual chirp [6].

The optical carrier is modulated to generate an optical field with the carrier and two sidebands in conventional intensity modulation. At the optical receiver, each sideband beats with the optical carrier, thereby generating two beat signals which constructively interfere to produce a single component at the RF frequency. However, if the signal is transmitted over fiber, chromatic dispersion causes each spectral component to experience different phase shifts depending on the fiber-link distance, modulation frequency, and the fiber-dispersion parameter. These phase shifts result in relative phase differences between the carrier and each sideband, and produce a phase difference in the two beat signals at the RF frequency, which results in a power degradation of the composite RF signal [7]. When the phase difference is kept equal to  $\pi$ , the complete cancellation of the RF signal occurs. As the RF frequency increases, the effect of dispersion is even more pronounced and the fiber-link distance severely limited [8,9]. Some types of external intensity modulators such as directional-coupler type modulator, loss modulator, Mach–Zehnder interferometer type modulator and total internal reflection type modulator have been studied [10]. Further, the measurement and influence of chirp parameter of MZM externally modulators over dispersion have been analyzed in fiber-wireless systems [11–13]. Smith et al. [14] demonstrated that the achievable link distance could be increased by varying the chirp parameter of the modulator to give large negative chirp using a dual-electrode Mach–Zehnder modulator (MZM) biased at quadrature. Kim and Gnauck [15] has investigated the chirp characteristics of dual-drive MZ modulators exhibiting a finite dc extinction ratio and found that the residual chirp could be minimized simply by driving the MZ modulator in a push–pull mode with unequal-amplitude signals.

In this work, the influence of extinction ratio with low chirp of MZM external modulators over RF power degradation introduced in RoF systems due to chromatic dispersion is reported which is not studied in earlier work. We discussed graphically, in Section 4 depending upon our simulative results obtained from Section 3, which reveals that RoF link can be improved and high quality microwave signal can be obtained by using SEMZM and DEMZM external modulators with low extinction ratio and chirp. The reduction in second order harmonic distortion (HD2) is also reported with low extinction ratio and chirp of MZM external modulators.

## 2. Theory

A continuous-wave (CW) signal from a laser is externally modulated using non-ideal DEMZM with non-identical loss introduced in each arm, which causes the finite extinction ratio  $\varepsilon_{LIN}$  of the device. The extinction ratio  $\varepsilon_{LIN}$  defines as the ratio between the output optical powers corresponding to the maximum transmission value and the one corresponding to the minimum transmission value. The output optical field at DEMZM is represented as

$$\vec{E}_{out} = 10^{-EL_{dB}/20} \left[ \cos \phi_D - \frac{j}{\varepsilon_{LIN}} \sin \phi_D \right] e^{j\phi_s} \cdot e^{j(\alpha \ln P_{out}/2)} \cdot \vec{E}_{in} \quad (1)$$

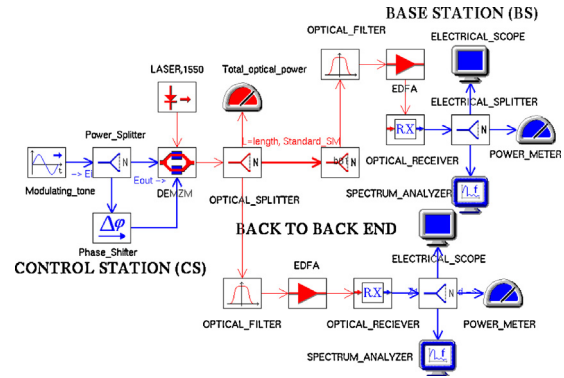


Fig. 1. Simulation setup using OPTSIM 4.6 for ODSB-RoF system.

where  $\alpha$  is the chirp parameter;  $V_{in} = (V_A - V_B)/2$ ;  $V_A$ ,  $V_B$  are the input voltages applied to the two arms of DEMZM modulator,  $\varepsilon_{dB} = 20 \log[\varepsilon_{LIN}]$ ,  $\phi_s = \pi/4[(V_A + V_B)/V_\pi]$ ,  $\phi_D = \pi/2[(V_{in} - V_0)/V_\pi] = \pi/2[(V_A - V_B - V_0)/V_\pi]$  and  $V_0$  is the offset voltage corresponding to the zero phase retardation in the absence of any electric field and is the value of the electrical input corresponding to the maximum transmission state. When the semi-difference between input voltages  $V_{in}$  is equal to  $V_0$ , the power of the optical signal is attenuated by the excess loss  $EL_{dB}$ , introduced by the modulator, so the modulator is said to be in maximum transmission state. Ideally, this value is 0 V, but often modulators become slightly unbalanced in the absence of any applied electric field. Thus, a biasing voltage must be applied to compensate the offset. To switch to the minimum transmission state, a  $V_\pi$  voltage must be added or subtracted to  $V_0$ .

To generate an optical SSB modulated signal, the DEMZM needs to be biased at the linear point,  $V_A - V_B = V_\pi/2$  with a phase shift between MZM drives of  $\phi_A - \phi_B = \pi[V_A/V_\pi] - \pi[V_B/V_\pi] = \pi/2$  that makes  $\phi_D = \phi_s = \pi/4$ . A significant advantage of the optical generation of high frequency electrical signals is the ease by which they can be distributed using optical fiber, without significant loss, over much greater distance than by using conventional electrical cables or waveguides. However, when this SSB optical modulated signal is transmitted over a single mode fiber (SMF), the chromatic dispersion of the fiber will cause an extra phase shift and introduce RF power degradations in RoF link expressed as [12]

$$P_{rf} \propto \cos \left[ \frac{\pi L D \lambda_c^2 f_{rf}^2}{c \{1 - (2/\pi) \arctan \alpha\}} \right] \quad (2)$$

where  $\alpha$  defines the frequency chirp of an external MZM modulator,  $D$  is the dispersion parameter,  $L$  is the length of the fiber,  $\lambda$  is the carrier wavelength,  $f_{rf}$  is fixed radio frequency.

## 3. Simulation setup

In our simulation set up schematically shown in Fig. 1, a RF signal of frequency 20 GHz is modulated by using either single- or dual electrode MZM (DEMZM) external modulator over a continuous wave (CW) laser at 1550 nm of laser line width 10 MHz with power of  $-2$  dB. The value of  $V_\pi$  for the single electrode modulator is measured as 13.0 V while the dual-electrode device has  $V_\pi = 8.2$  V. The optimum operating point was achieved by biasing at quadrature  $\gamma = \pi/2$ , i.e., which is defined as the mid-point of the normalized spread of the transfer function of MZM and applying an RF signal of 20 GHz with a drive level of  $0.45 V_\pi$ . The offset voltage  $V_0$  corresponding to the zero phase retardation in the absence of any electric field is 0 V, ideally. But, usually, external modulators become slightly unbalanced in the absence of any applied electric

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