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# Effect of temperature tuning on the aerosol acoustic aggregation process

### <sup>Q3</sup> Q2</sup> Zhenghui Qiao<sup>1</sup>, Wei Dong<sup>1,2,\*</sup>, Yaji Huang<sup>1</sup>, Vincenzo Naso<sup>2</sup>

- 4 1. Key Laboratory of Energy Thermal Conversion and Control of Ministry of Education, School of Energy & Environment, Southeast University,
- 5 Nanjing 210096, China. E-mail: seuqzh@seu.edu.cn
- 6 2. Department of Mechanical and Aerospace Engineering, SAPIENZA University of Rome, Via Eudossiana, 18-00184 Rome, Italy
- 7

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#### ABSTRACT

Diesel exhaust aerosols (DEAs) can absorb and accumulate toxic metal particulates and bacteria 16 suspended in the atmospheric environment, which impact human health and the environment. 17 The use of acoustic standing waves (ASWs) to aggregate DEA is currently considered to be an 18 efficient particle removal method; however, study of the effect of different temperatures on the 19 acoustic aggregation process is scarce. To explore the method and technology to regulate and 20 optimize the aerosol aggregation process through temperature tuning, an acoustic apparatus 21 integrated with a temperature regulation function was constructed. Using this apparatus, the 22 effect of different characteristic temperatures (CTs) on the aerosol aggregation process was 23 investigated experimentally in the ASW environment. Under constant conditions of acoustic 24 frequency 1.286 kHz, voltage amplitude 17 V and input electric power 16.7 W, the study 25 concentrated on temperature effects on the aggregation process in the CT range of 58–72°C. The 26 DEA opacity was used. The results demonstrate that the aggregation process is quite sensitive to 27 the CT, and that the optimal DEA aggregation can be achieved at 66°C. The aggregated particles 28 of 68.17 µm are composed of small nanoparticles of 13.34-62.15 nm. At CTs higher and lower 29 than 66°C, the apparatus in non-resonance mode reduces the DEA aggregation level. For other 30 instruments, the method for obtaining the optimum temperature for acoustic agglomeration is 31 universal. This preliminary demonstration shows that the use of acoustic technology to regulate 32 the aerosol aggregation process through tuning the operating temperature is feasible and 33 34 convenient.

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#### 49 Introduction

The diesel engine, as a type of combustion engine, is widely used in transportation areas, and has become a troublesome soot emitter for the atmospheric environment. Numerous diesel exhaust aerosols (DEAs), commonly with submicron size, (Guan et al., 2015; Burtscher, 2005; Kittelson, 1998; Harris and Maricq, 2001; Wang et al., 2012) are exhausted into the environment, which exacerbates the atmospheric particle pollution, such as the particulate matter of diameter less than 58 2.5  $\mu$ m (PM<sub>2.5</sub>) level. Acoustic removal (Chen et al., 2009, 2015; 59 Gallego-Juarez et al., 1999; González et al., 2003; Guo et al., 2012; 60 Liu et al., 2009, 2011; Noorpoor et al., 2012; Sheng and Shen, 2007; 61 Sun et al., 2013; Yuen et al., 2014) enhances the growth process 62 from small to large aerosol particles by means of acoustic 63 standing waves (ASW) impacts. The process through which the 64 ASW interacts with DEA is generally referred to as acoustic 65 aggregation. Chen et al. (2009) found that the particle size 66

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<sup>\*</sup> Corresponding author. E-mail: dongwei59@seu.edu.cn (Wei Dong).

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67 distribution of the ultrafine particles in diesel engine exhaust can be markedly changed by ASW at room temperature. 68 69 Noorpoor et al. (2012) asserted that the ASW field can coagulate 70 nano-particles in diesel exhaust in order to become larger size under any temperature condition. In addition, many re-71 72 searchers, for example, Chen et al. (2015), Sun et al. (2013), Guo et al. (2012), Liu et al. (2009, 2011) and Gallego-Juarez et al. (1999), 73 have verified that coal-fired flue ash can be significantly 74 75 removed by an enhanced process of acoustic aggregation. 76 Chen et al. (2015) proposed that the coupling of the acoustic 77 and electric environment can efficiently remove fine particles 78 from coal combustion. Yuen et al. (2014) proposed that 79 nonlinear acoustics can act as an energy-efficient technique to enhance the aerosol removal process. Sun et al. (2013) proposed 80 that the coupling effect between a gas jet and acoustic wave can 81 also efficiently remove coal-fired particles. Qiao et al. (2015) 82 proposed that the structural parameters of the acoustic 83 resonant field can enhance the spatial distribution of aerosols 84 and result in the X-pattern distribution phenomenon. In the 85 above studies, temperature is commonly considered as an 86 87 important factor (Noorpoor et al., 2012; Sheng and Shen, 2007; Liu et al., 2009; González et al., 2003) impacting the effect of 88 aerosol removal in an ASW field, yet relevant experimental 89 90 studies investigated the removal process under a constant temperature condition. Study on the effect of different temper-91 92 atures on the removal process is scarce. Considering the 93 importance of the temperature factor on the acoustic aggrega-94 tion process, it is necessary to study the potential effects of 95 temperature on the aerosol aggregation process in an acoustic 96 field, which is the objective of this paper.

97 In recent studies on aerosol removal by ASW (Chen et al., 2009, 2015; Gallego-Juarez et al., 1999; Guo et al., 2012; Liu et al., 2009, 98 99 2011; Noorpoor et al., 2012; Qiao et al., 2014, 2015; Sheng and Shen, 2007; Sun et al., 2013; Yao et al., 2010; Yuen et al., 2014), the 100 particle size distribution is generally considered an indispensable 101 102 factor to reflect the change of aerosol behavior characteristics. One important reason is that smaller aerosols (such as those with 103 particle size less than 2.5 µm) cannot be completely removed by 104 105 the traditional particle removal apparatus (Yao et al., 2010). The second is that the particle size distribution of aerosols can clearly 106 change under the influence of ASW. In addition, aerosol opacity is 107 an important index to determine the concentration of aerosols 108 (Kumar et al., 2005; Zajac, 2008; Czechlowski et al., 2015). The 109 mechanism is based on the light penetrability of smoke with 110 111 different aerosol concentrations. A higher opacity corresponds to 112 a higher concentration of aerosol. Notably, the aerosol opacity is currently considered as a control index to assess the emission 113 performance of diesel exhaust (Sae, 1996). Accordingly, in this 114 paper we will utilize the opacity to characterize the aerosol 115 concentration variation with different characteristic tempera-116 tures (CTs) given by a temperature tuning platform. 117

In our previous study, we invented a new apparatus for 118 generating an ASW field (Qiao et al., 2014, 2015). The perfor-119 120 mance in aerosol removal has been tested for tobacco smoke 121 (Qiao et al., 2014). Based on the apparatus, a new apparatus for generating an ASW field with optimal temperature control was 122 123 constructed to explore the effect of temperature on the acoustic aggregation process for DEA. The DEA aggregation process was 124 investigated at six different CTs in the range of 58-72°C. The 125 corresponding DEA opacity variation was used to evaluate the 126

effect on the DEA aggregation process. Especially, we empha- 127 size the interesting potential of the enhancement of the 128 acoustic aggregation level by means of temperature tuning. 129

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#### 1. Experiment and method

#### 1.1. Experimental apparatus

The laboratory experimental unit was constructed, and the main 133 configuration of the acoustic apparatus with the temperature 134 tuning platform is shown in Fig. 1. The composite image 135 composed of images A, B and C simply represents the apparatus 136 configuration for generating an ASW field with optimal temper- 137 ature control. The ASW field in the cylindrical aerosol chamber 138 (CAC) is regulated and controlled with a pair of opposing 139 Helmholtz resonant sources (HRS) composed of a Helmholtz 140 resonator (HR) and speaker (Qiao et al., 2014, 2015). The HRS based 141 on acoustic streaming causes a large acoustic pressure. The 142 dashed arrow demonstrates the supply process for the sinusoidal 143 alternating-current (AC) voltage signal from the signal generator 144 and amplifier to the speaker. The temperature tuning platform 145 composed of heating tape, temperature controller and thermo- 146 couple has the function of conveniently regulating and control- 147 ling the heating temperature. The heating tape is wrapped on the 148 wall of the CAC to form a steady operating temperature 149 environment in it. The heating temperature of the heating tape 150 is regulated by the temperature controller by manipulating the 151 warming-up time. The thermocouple for measuring CT is 152 mounted on the interface between the heating tape and the 153 outside surface of CAC at position D (see image B). The dash dot 154 line demonstrates the process of temperature regulation and 155 control. The double dash line represents the signal wire of the 156 thermocouple. The opacity measurement system consists of a 157 smoke opacity meter (SV-5Y, Tianjin Shi Shengwei Development 158 of Science Company Limited, China) and exhaust gas analyzer 159 (SV-5Q, Tianjin Shi Shengwei Development of Science Company 160 Limited, China). The sampling probe of the smoke opacity meter 161 is inserted into the cushion chamber to extract DEA. The opacity 162 data measured by the smoke opacity meter is analyzed and 163 recorded by the exhaust gas analyzer. The measured precision of 164 the opacity is  $\pm 0.2\%$ . The solid line arrow demonstrates the flow 165 direction of diesel exhaust in each component. At the smoke 166 entrance of position F (see image C), the smoke exhausted from 167 diesel is drawn into the CAC by an exhaust separator. After the 168 action of ASW field at a specific temperature condition in CAC, 169 the diesel exhaust is discharged into the cushion chamber. The 170 cushion chamber is used for the DEA sampling of the opacity 171 measurement system. The smoke output of the CAC is arranged 172 at position E (see image A), as the sampling point for the opacity 173 measurement. This point represents the average position be- 174 tween the adjacent nodal point and anti-nodal point of ASW. 175

For the experiment parameters of the diesel engine, the 176 torsion is 19.9 N/m, and the load is 17%; the engine speed is 177 1204 r/min; the power is 2.51 kW; the fuel consumption is 178 403.5 g/kWh. For the experimental parameters of the acoustic 179 sources, the voltage amplitude and the total electrical power 180 input of the signal supplied from the amplifier to the speakers is 181 17 V and 16.7 W, respectively. During the acoustic aggregation 182 experiment at all CTs, the acoustic frequency is constant, always 183

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