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Combined zero valent iron and hydrogen peroxide conditioning significantly enhances the dewaterability of anaerobic digestate

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Introduction

ABSTRACT

The importance of enhancing sludge dewaterability is increasing due to the considerable 23 impact of excess sludge volume on disposal costs and on overall sludge management. This 24 study presents an innovative approach to enhance dewaterability of anaerobic digestate 25 (AD) harvested from a wastewater treatment plant. The combination of zero valent 26 iron (ZVI, 0–4.0 g/g total solids (TS)) and hydrogen peroxide (HP, 0–90 mg/g TS) under pH 3.0 27 significantly enhanced the AD dewaterability. The largest enhancement of AD dewaterability 28 was achieved at 18 mg HP/g TS and 2.0 g ZVI/g TS, with the capillary suction time reduced by 29 up to 90%. Economic analysis suggested that the proposed HP and ZVI treatment has more 30 economic benefits in comparison with the classical Fenton reaction process. The destruction 31 of extracellular polymeric substances and cells as well as the decrease of particle size were supposed to contribute to the enhanced AD dewaterability by HP + ZVI conditioning. 33 © 2017 The Research Center for Eco-Environmental Sciences, Chinese Academy of Sciences. 34

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The most commonly used technology for wastewater treatment is the activated sludge process. However, a huge amount of excess sludge is generated in this process, which causes environmental problem (Foladori et al., 2010; Wang et al., 2013a, 2013b; Zhao et al., 2016). Nowadays, excess sludge management is one of the major challenges in wastewater treatment plants (WWTPs). In fact, treatment and disposal of excess sludge incurs large expenditures, which occupy up to 56 30%–60% of the total cost of a WWTP (Foladori et al., 2010; Wang 57 et al., 2017). 58

The sludge treatment and disposal procedure usually 59 encompasses thickening, stabilization, conditioning, dewatering 60 and disposal (Foladori et al., 2010). Dewatering has been proven to 61 be an efficient method to reduce sludge volume, cutting sludge 62 transport and disposal cost. Since sludge has poor dewaterability, 63 conditioning process is commonly used to enhance the sludge 64

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dewaterability prior to dewatering (Wang et al., 2013c). Sludge 65 comprises free water and bound water. The free water combines 66 with the sludge structure in a loose manner and hence is able to 67 be removed much more easily during the dewatering process. 68 On the contrary, the bound water is combined with the sludge 69 via capillary forces or chemical bonds, which is much more 70 difficult to be eliminated compared with the free water. Sludge 71 conditioning could transform the bound water in sludge into the 72 73 free water to enhance sludge dewaterability (Wang et al., 2014; Li 74 et al., 2016; Liu et al., 2016a, 2016b; Zhang et al., 2016).

Until now, a number of approaches for sludge condition-75ing have been investigated. They include classical Fenton 76 reaction treatment, alkaline or acid treatment, flocculation agent 77 addition, freezing and heat treatment (Wang et al., 2014; Gong 78 et al., 2015; Li et al., 2016; Liu et al., 2016a, 2016b; Zhang et al., 79 2016). Amongst them, Fenton reaction is an excellent approach 80 because it is striking in improving sludge dewaterability (Liang 81 et al., 2015; He et al., 2015). The classical Fenton reaction is 82 composed of a series of reactions between Fe²⁺ and hydrogen 83 peroxide (HP) under acid condition (Eqs. (2)-(8)) (Pignatello et al., 84 2006). In these reactions, huge amount of hydroxyl radical (HO.) 85 is generated (Eq. (2)), which is a much stronger oxidant in 86 comparison to HP (Nevens et al., 2003). When the sludge contacts 87 88 with hydroxyl radicals, the structure of the sludge is effectively 89 changed and microorganisms would be decomposed by oxida-90 tion. This will improve the sludge dewaterability by facilitating 91 the sludge conditioning (Tony et al., 2008; Fontmorin and 04 Sillanpaa, 2015).

$$93 \qquad Fe + 2H^+ \rightarrow Fe^{2+} + H_2 \tag{1}$$

 $Fe^{2+} + H_2O_2 \rightarrow Fe^{3+} + HO^{-} + OH^{-}$ 96 $Fe^{3+} + H_2O_2 \rightarrow Fe^{2+} + HOO^{\cdot} + H^+$ 98 $HO \cdot + H_2O_2 \rightarrow HO_2 \cdot + H_2O_2$ (4)900 $HO \cdot + Fe^{2+} \rightarrow Fe^{3+} + OH^{-}$ (5)107 $Fe^{3+} + HO_2 \cdot \rightarrow Fe^{2+} + O_2H^+$ (6)104 $Fe^{2+} + HO_2 \cdot + H^+ \rightarrow Fe^{3+} + H_2O_2$ (7)106 $HO_2 \cdot + HO_2 \cdot \rightarrow H_2O_2 + O_2$ (8)

Nevertheless, the Fe²⁺ is instable compared with zero 109 valent iron (ZVI). ZVI was able to be oxidized to Fe²⁺ by acid 110 111 as a result of its highly reductive characteristics (Eq. (1)). Therefore, ZVI was also able to get involved in the Fenton-like 112reactions at acidic condition (Eqs. (1)-(8)). Recently, the 113HP-ZVI system has been investigated to enhance the excess 114 sludge dewaterability (Zhou et al., 2014). The capillary suction 115 time (CST) of excess sludge, which is an indicator of sludge 116dewaterability, was decreased by around 50% using com-117 bined HP and ZVI conditioning (Zhou et al., 2014). However, 118 119 excess sludge usually undergoes anaerobic digestion before 120 dewatering in most WWTPs, to produce biogas and reduce excess sludge (Foladori et al., 2010; Bacenetti et al., 2013). 121 After this, huge quantities of anaerobic digestate (AD) are still 122produced, which needs to be dewatered before its final 123 disposal. Nevertheless, the dewatering performance of AD is 124 of great difference compared with that of excess sludge 125

because of the different characteristics between AD and 126 excess sludge (Foladori et al., 2010; Zhang et al., 2015). 127 Therefore, the efficient conditioning approach for enhancing 128 AD dewaterability deserves to be explored. 129

This work aims to systematically evaluate the effective- 130 ness of the HP-ZVI conditioning in the AD dewaterability. To 131 the best of our knowledge, it is the first time that the HP-ZVI 132 treatment is employed as an AD conditioning approach to 133 improve AD dewaterability. The AD dewaterability indicator, 134 that is CST, was measured before and after HP-ZVI condi- 135 tioning. The concentrations of dissolved iron in AD were 136 determined before ZVI-HP conditioning and after ZVI recov- 137 ery. Soluble chemical oxygen demand (SCOD) concentration 138 in AD was also measured after HP-ZVI conditioning. The 139 economic potential of the HP-ZVI conditioning approach was 140 determined. 141

1. Materials and methods

The AD was collected from the anaerobic sludge digester of a 145 local biological nutrient removal WWTP. The main characteris- 146 tics of AD are as following: iron 320 \pm 5 mg/L, total solids (TS) 147 22.3 \pm 0.4 g/L, volatile solids (VS) 19.1 \pm 0.2 g/L, solid content 148 2.23% \pm 0.04%, moisture content 97.77% \pm 0.04%, chemical oxygen 149 demand (COD) 22.1 \pm 0.2 g/L, CST 115.6 \pm 0.7 sec, and pH 7.72. 150 ZVI power (size: 80 meshes; Australian Metal Powder 151

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Supplies Pty Ltd.) was adopted in this work. The concentration 152 of HP stock solution (Ajax Finechem Co.) was 33%. 30% sulfuric 153 acid was utilized to adjust the AD pH. 154

1.2. Batch experiments

Two groups of batch experiments were carried out to investigate 156 the effects of HP and ZVI levels on the dewaterability of AD, 157 which is shown in Table 1. The first group was to evaluate the 158 effect of ZVI concentrations (0–4.0 g/g TS) when HP concentration 159 was kept at 90 mg/g TS. The second group aimed to evaluate the 160 effect of HP concentrations (0–90 mg/g TS) while the concentra-161 tion of ZVI was kept at 2.0 g/g TS. All the experiments were 162 prepared and analyzed in duplicate in this work. 163

Table 1 – Experimental conditions used in the HP-ZVI enhanced AD dewaterability experiments.			t1.1 t1.2
Group	HP concentration (mg/g TS)	ZVI concentration (g/g TS)	t1.3 t1.4
I. Effect of ZVI	90	0	t1.5
concentration	90	0.25	t1.6
	90	0.5	t1.7
	90	1.0	t1.8
	90	2.0	t1.9
	90	4.0	t1.10
II. Effect of HP	0	2.0	t1.11
concentration	18	2.0	t1.12
	45	2.0	t1.13
	90	2.0	t1.14
ZVI: zero valent iron; HP: hydrogen peroxide; TS: total solids.			t1.16

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