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Pulsed corona discharge for improving treatability of coking wastewater

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ABSTRACT

Coking wastewater (CW) contains toxic and macromolecular substances that inhibit 17 biological treatment. The refractory compounds remaining in biologically treated coking 18 wastewater (BTCW) provide COD and color levels that make it unacceptable for reuse or 19 Q9 disposal. Gas-phase pulsed corona discharge (PCD) utilizing mostly hydroxyl radicals and 20 ozone as oxidants was applied to both raw coking wastewater (RCW) and BTCW wastewater 21 as a supplemental treatment. The energy efficiency of COD, phenol, thiocyanate and cyanide 22 degradation by PCD was the subject of the research. The cost-effective removal of 23 intermediate oxidation products with addition of lime was also studied. The energy 24 efficiency of oxidation was inversely proportional to the pulse repetition frequency: lower 25 frequency allows more effective utilization of ozone at longer treatment times. Oxidative 26 treatment of RCW showed the removal of phenol and thiocyanate at 800 pulses per second 27 from 611 to 227 mg/L and from 348 to 86 mg/L, respectively, at 42 kWh/m³ delivered energy, 28 with substantial improvement in the BOD₅/COD ratio (from 0.14 to 0.43). The COD and color 29 of BTCW were removed by 30% and 93%, respectively, at 20 kWh/m³, showing energy 30 efficiency for the PCD treatment exceeding that of conventional ozonation by a factor of 3-4. 31 Application of lime appeared to be an effective supplement to the PCD treatment of RCW, 32 degrading COD by about 28% at an energy input of 28 kWh/m³ and the lime dose of 3.0 kg/m³. 33 The improvement of RCW treatability is attributed to the degradation of toxic substances 34 and fragmentation of macromolecular compounds. 35 © 2017 The Research Center for Eco-Environmental Sciences, Chinese Academy of Sciences. 36

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49 Introduction

51 Coking wastewater (CW) is generated from coke quenching, 52 coking gas purification and the recovery of chemical products 53 from coking tar, gas and water (Schobert and Song, 2002). It has 54 a large variety of constituents, including refractory organic 55 compounds of poor biodegradability (Lu et al., 2009). These 56 compounds comprise organic loads with excessive levels of bio-inhibition and genotoxicity for biological treatment 57 (Young et al., 2008; Dong and Zhang, 2010). The refractory **Q10** constituents, such as phenolic compounds, polyaromatic 59 hydrocarbons (PAHs) and inorganic thiocyanate and cyanide, 60 were proven to have high toxicity toward most microorgan- 61 isms (Kwon et al., 2002; Young et al., 2011; Sharma et al., 2012). **Q11** For example, highly toxic phenol in aqueous media is severely 63 restricted by current legislation (CJ 343–2010); its presence 64

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inhibits bacterial degradation of thiocyanate with Acremonium 65 strictum (Kwon et al., 2002). In biological treatment, phenol in 66 concentrations exceeding 200 mg/L significantly inhibits ni-67 trification, stopping it completely at concentrations above 68 500 mg/L. Low concentrations of phenol, on the other hand, 69 negatively affect nitrification indirectly by oxygen depletion 70 due to the fast growth of heterotrophic phenol-degrading 71 bacteria (Sharma and Ahlert, 1977). The wastewater was found 72 73 to contain a minimum of fifteen identified phenolic com-74 pounds (Ly et al., 2015). According to Kim et al. (2011), a free cyanide concentration above 0.2 mg/L causes serious inhibi-75tion of CW nitrification. Thiocyanate shows toxicity similar to 76 that of phenol: a concentration of 200 mg/L noticeably inhibits 77 nitrification in activated sludge, resulting in poor removal of 78 nitrogen (Kim et al., 2008). As a result, the CW biodegradability 79 as described by the BOD₅/COD ratio usually does not exceed 0.3 012 (Zhou et al., 2014). 81

The biological processes used in CW treatment include 82 anaerobic digestion (A) combined with aerobic oxidation (O) in 83 various sequences described in the literature under various 84 A/O-names, such as two-stage anaerobic–aerobic (A²/O), anaer-85 obic-aerobic-hydrolytic-aerobic (A/O1/H/O2), sequential biolog-86 ical reactors (SBR) etc. (Li et al., 2003; Marañón et al., 2008; Lu 87 88 et al., 2009; Yu et al., 2015). The A/O1/H/O2 sequence is applied at the target site, the Guangdong Shaoguan Steel Company, 89 90 providing the CW samples for this study. The anaerobic 91 bioreactors reduce the toxicity and improve the BOD5/COD 92ratio for further aerobic oxidation. Even free cyanide may be removed by anaerobic bacteria, making anaerobic digestion a 93 powerful means of treatability enhancement (Shieh and 94Richards, 1988). However, the hydraulic retention time (HRT) 95 in aerobic bioreactors is long, reaching up to 24 hr, resulting in 96 substantial need for compressed air, i.e. energy consumption 97 (Zhu et al., 2016). As a result, biological treatment often does not 98 meet the National Discharge Standard of China (GB 16171-2012). 99 The discharged CW must not exceed a COD of 80 mg O₂/L, i.e. 100 the industry faces the need in removal of 40%-50% of the 101 residual COD of biologically treated CW (BTCW). Achieving the 013 target lies in the reduction of the CW toxicity, enabling deeper 103 and faster biological degradation of organic pollutants. 104

Improvement of the CW treatability is normally achieved 105106 through toxicity alleviation, fragmentation of large-size mole-107 cules and liberation of organic nitrogen into easily digested ammonia or nitrate (Dong and Zhang, 2010; Sun et al., 2015). 108 Various biological and physicochemical methods have been 109 developed to improve CW treatability, including biofilm sys-110 tems (Qian and Liu, 2016), supercritical and sub-critical catalytic 111 wet air oxidation pre-treatment (Chen et al., 2012; Du et al., 1122013), electrochemical degradation (Wang et al., 2008; Fuat and 113 Bunyamin, 2015), Fenton oxidation (Chu et al., 2012), and 114 ozonation (Duan et al., 2015). Chemical oxidation targets the 115improvement of treatability by means of all the above-116 mentioned transformations - reduced wastewater toxicity, 117 fragmentation of poorly biodegradable molecules and releasing 118 ammonia from nitrogen-containing organic pollutants. Combi-119 nations of biological, physicochemical, and physical treatment 120121methods have been developed to achieve the emission standards (Lai et al., 2009; Jin et al., 2013; Sharma and Philip, 2016), although 122so far these have not been applied commercially for economic 123 and performance reasons. For example, the severe process 124

conditions and high investment costs in wet air oxidation limit 125 its application to large-scale enterprises treating highly concen- 126 trated wastewaters. Fenton oxidation, requiring substantial 127 doses of hydrogen peroxide, results in bulk amounts of ferric 128 hydroxide precipitates (Namkung et al., 2008). Electrolysis 129 combined with ozone shows attractive results in COD degrada- 130 tion energy efficiency, from 15 to 32 g O₂/kWh (Kwiecińska et al., 131 2016), although the abundance of chloride ions in CW 132 (Słomka-Słupik and Zybura, 2015; Kwiecińska et al., 2016) results 133 in the inevitable formation of refractory and toxic halocarbons 134 (Szpyrkowicz et al., 2001), reducing the biodegradability. 135 Pre-ozonation of diluted CW in a lab-scale reactor, although it 136 improved the biodegradability, required hours to achieve results, 137 making the expected energy expense prohibitive (Duan et al., 138 2015). There is also a report on preliminary ozonation having a 139 negative effect on biodegradability (Chang et al., 2008). Such 140 contradictory examples indicate the necessity of verifying the 141 effect of pre-oxidation on the subsequent biological treatability 142 of CW. 143

Gas-phase pulsed corona discharge (PCD), also known as 144 low-temperature plasma, produces highly reactive short-lived 145 oxidants when applied to an oxygen- and water-containing 146 gas (Ono and Oda, 2003): 147

$\bar{e} + H_2 O \rightarrow \bar{e} + H + OH$	(1)
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 $O(^{1}D) + H_{2}O \rightarrow 2^{\cdot}OH$ (2) 148

$$\bar{e} + 3O_2 \rightarrow \bar{e} + 2O_3$$
 (3)

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Operated in gas-liquid mixtures, in which treated water is 154 showered onto the electrodes, PCD showed the highest energy 155 efficiency among advanced oxidation processes (AOPs) in 156 oxidation of various pollutants of high (Preis et al., 2013) and 157 low oxidation rates (Panorel et al., 2011; Ajo et al., 2015), 158 surpassing the conventional ozonation by at least a factor of 159 two. This efficiency is achieved by utilizing short-lived powerful 160oxidants, mainly hydroxyl radicals, generated at the surface of 161 the treated water (Preis et al., 2013). Ozone formed in the 162 discharge assists oxidation, where its oxidation potential is 163 sufficient (Kornev et al., 2014). Other advantages include the 164 insensitivity of PCD toward the gas humidity, the possibility of 165 using elevated concentrations of oxygen, the lack of need for 166 gas transport and, thus, residual ozone destruction (Preis et al., 167 2013). The extent of pollutant oxidation is controlled by 168 regulation of the pulsed discharge energy dose to control the 169 subsequent treatability of the wastewater. The ratio of 170 'OH-radical-ozone' usage is adjusted by the pulse repetition 171 frequency, controlled over a wide range (Preis et al., 2013). 172

In the present research, PCD was for the first time studied in 173 the treatment of CW, aiming for the improvement of its 174 biodegradability and treatability in combined technology appli-175 cations. The combination of treatment methods used for 176 heavily polluted wastewaters may also include the removal of 177 organic compounds of, for example, acidic nature by settling 178 with low-cost chemicals, such as coagulants and lime (Hill et al., 179 1979; Sevimli et al., 2000). The effect of precipitation of oxidation 180 products was pronounced in the sequential combination of 181 preliminary oxidation with application of lime (Munter et al., 182 1987), also tested in the present research in respect to raw 183 coking wastewater (RCW).

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