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Research paper

Work patterns, capacity and cost of rice combine

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ABSTRACT

The mechanization of rice production is important, especially for harvesting. To improve the work capacity and reduce the operating cost of rice combines, we studied the work patterns and the operating efficiency of the machinery. The factors affecting operating costs were evaluated.

To study the effect of two harvesting patterns – circuitous and continuous on the efficiency of rice combine; we estimated a series of work locus equations. Work efficiency and capacity were defined by the area of the paddy field, type of machinery, and work patterns. With field area <0.4 ha, a circuitous pattern was efficient. With fields 0.4-0.5 ha, either pattern could be used. A continuous pattern was efficient for larger areas.

Operating capacity and purchase price were the major factors determining operating cost. In terms of long-term development, a larger combine is more economical.

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1. Introduction

Harvesting is the most important farm work in rice production. In 2014, about 99% of rice paddies in Taiwan were harvested by machinery. To increase the operation areas, machinery-owners work for themselves and neighbors. The fee for paddy field harvesting paid to the machinery-owner is called the custom service rate. Because of the prevalence of the custom work system, the typical work hours per year for rice combines is high so the depreciation period is reduced (Kamboj et al., 2012). Improving work capacity and reducing the operating cost of rice farming requires studying the work patterns and the efficiency of rice combines. The factors affecting operating costs need to be evaluated.

Hunt (1973) described different work patterns for large farm equipment in the Unites States. In addition, farm machinery costs have been estimated (Hassan et al., 1978; Kepper et al., 1994; Renoll, 1981; Robb et al., 1988). Also, Salassi and Deliberto (2010) proposed one set of software to calculate the operating costs of rice combines.

The study of work patterns of the harvesting machinery in Japan included only two-row riding-type combines (Shimizu and Fukayama, 1971). Busato et al. (2007) modelled the efficiency of combines for the interaction of work patterns and field bin positions to improve the efficiency of transportation.

In this study of work capacity, we modeled work patterns for rice combines as a series of equations, investigated related parameters and substituted into equations to find the work efficiency of three types of combines. The cost of rice combines was divided into fixed and variable costs. Five types of machinery were compared.

2. Model development

2.1. Work patterns and capacity

To utilize a rice paddy field effectively, no unprocessed land of paddy field should be left for headland. Before harvesting, the fields need to be reaped by hand at the four corners and around the four sides to provide enough turn strips for operating of machinery (Fig. 1). All reaped grains are threshed by the combine thresher.

2.1.1. Work methods

The first stage involves harvesting around the field sides to obtain enough headland and for the next stage (Fig. 2). Turning a 90° corner required time. The second stage involved two different patterns: circuitous and continuous.

a. Circuitous pattern (Fig. 3)

With a residual field width (W_1) was <20 m, the combine circle around the work area as shown in Fig. 2. The field length for

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Notation		Ps	salvage value, NT\$
		Pt	total travelled paths, m
A _h	headland area, m ²	r	average ratio value for oil cost
а	length of headland, m	R _c	repair cost per year, NT\$/yr
b	width of headland, m	S	operating velocity for the combine, m/sec
Cm	manual capacity of reaping by hand, sec/m ²	Sm	operating capacity for the thresher to thresh the grains
Cr	total repair coefficient		reaped by hand, sec/m ²
D _c	annual depreciation charge, NT \$/yr	Ta	total annual work area, ha
Fc	estimated cost of fuel, NT\$/yr	Te	theoretical total work time, sec
Ef	operating efficiency	Ti	total work time for the whole field operation, sec
Fo	field operating capacity, ha/hr	Tf	time to turn a 90° corner, sec
Н	annual operating hours, hr/yr	T _h	manual reap-time for the headland, sec
hp	horsepower of the rice combine	Ts	required time to thresh the grains, sec
i	annual interest rate	T _{ui}	required turning time for the "U" -type rotation of
I _c	interest cost per year, NT\$/yr		circuitous pattern, sec
Κ	number of sub-regions with the same width	Tr	time for turning of 180, sec
K _f	fuel consumption coefficient	Tw	total economic work hours for this machinery, hr
L	length of paddy field, m	T ₁	required operating time for this first stage, sec
Lc	annual labor cost, NT \$/yr	T ₂	required operating time for circuitous pattern with
Lw	hourly wage, NT\$/hr		$W_1 < 20 m, sec$
L ₁	residual field length, m	T ₃	required operating time for circuitous pattern with
Ny	estimated economic years of life, yr		$W_1 > 20$ m, sec
N_1	required circuit number for the first stage	T_4	total operating time for continuous pattern, sec
N_2	required time for rotation times of circuitous pattern	W	effective operating width of combine, m
	with $W_1 < 20 \text{ m}$	W	width of paddy field, m
N ₃	required time for rotation times of circuitous pattern	W _h	width of the manual reaped around four sides, m
	with $W_1 > 20 \text{ m}$	W_{s1}	some sub-regions have equal width with $W_1 > 20$ m
N_4	total required rotation times for continuous pattern		for circuitous pattern, m
Oc	lubricant oil costs	W_{s2}	smallest sub-region width with $W_1 > 20$ m for
Pc	purchase price, NT\$		circuitous pattern, m
Pm	required labor	W_1	residual field width, m

harvesting was fixed at L_l.

With $W_1 > 20$ m, the residual work field is divided into several sub-regions with width 10–12 m. The sub-regions are harvested by inner- or outer-circular patterns (Fig. 3). As the combine finishes one long side, it turns along a "U" -type path to the next starting point.

b. Continuous pattern (Fig. 4)

After the first stage, rice is harvested by a continuous pattern. Each time requires a 180° turn at a limited distance.

2.1.2. Analysis of required time

a. Headland area and operation time

The headland area, A_h (m²), can be calculated as follows:

$$A_{h} = 4a^{*}b + 2W_{h}^{*}(L + W - 2a - 2b)$$
(1)

where a = length of headland (m).

$$\begin{split} b &= width \ of \ headland \ (m), \\ W_h &= width \ of \ the \ manual \ reaped \ around \ four \ sides \ (m), \\ W &= width \ of \ paddy \ field \ (m) \ and \\ L &= length \ of \ paddy \ field \ (m). \end{split}$$

The manual reap-time for the headland was T_h (sec),

$$T_h = A_h^* C_m \tag{2}$$

where $C_m =$ manual capacity of reaping by hand (sec/m²). The required time to thresh the grains was T_s (sec),

$$\Gamma_{\rm s} = A_{\rm h}^* S_{\rm m} \tag{3}$$

where $S_m =$ operating capacity for the thresher to thresh the grains reaped by hand (sec/m²).

b. Operating time for the first stage

The travel paths of the combine during the first stage are in Table 1.

The total travelled paths was $P_t(m)$,

$$P_{t} = 2^{*}N_{l}^{*}(L + W) - 4^{*} w^{*} N_{1}^{2}$$
(4)

where N_1 = required circuit number for the first stage and

w = effective operating width of combine (m).

The required operating time for this first stage was T_1 (sec),

$$T_1 = (2 * N_1 * (L + W) - 4 * N_1^2 * W)/s + 4 * N_1 * T_f$$
(5)

where s = the operating velocity for the combine (m/sec) and

 $T_f=$ the time to turn a 90° corner (sec).

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