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Conservative Upwind Difference Schemes for Open Channel Flows—Theory and Applications

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Abstract—Conservative upwind finite-difference schemes are presented for the solution of the onedimensional shallow water equations in open channels Numerical results are presented and compared for different versions of the schemes when applied to a test problem comprising a channel with varying breadth and depth and friction terms. This includes consideration of the effect of treating part of the flux balance as a source, and a comparison of square-root and arithmetic averaging (© 2005 Elsevier Ltd. All rights reserved.

Keywords-Shallow water equations, Upwinding, Conservation, Source terms

1. INTRODUCTION

In a recent paper [1], four different versions of a numerical upwind scheme for the one-dimensional shallow water equations were considered. The schemes were all based on flux balance distribution methods, and the governing equations were the St. Venant equations for flow in a friction-less channel of uniform rectangular cross-section. The schemes were compared by applying them to a standard dam-break problem. In this paper, we extend the schemes to the St. Venant equations incorporating variable breadth, depth, and friction terms, and present a numerical comparison of the schemes when applied to a test problem encompassing these features.

2. THE GOVERNING EQUATIONS

The St. Venant equations [2] governing the rough-turbulent flow of water in an open channel can be written in conservation form as

$$\underline{w}_t + \underline{f}_x = \underline{s},\tag{2.1}$$

where

$$\underline{w} = \left(A, Q\right)^{\mathsf{T}} \tag{2.2}$$

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are the conserved variables, the flux function,

$$\underline{f}(\underline{w}) = \left(Q, Q^2/A\right)^{\top} \tag{2.3}$$

and the source term,

$$\underline{s}(\underline{w}) = \left(0, -gA\left(\frac{\partial h}{\partial x} + Q|Q|/K^2\right)\right)^{\prime}.$$
(2.4)

These equations represent conservation of mass and momentum, and the source term <u>s</u> arises through the variation in the channel bottom and frictional effects. The quantities A = A(x,t)and Q = Q(x,t) = Au(x,t) represent the cross-sectional area and mass flow, respectively, at a general position x measured along the channel, and at time t, where u is the fluid velocity. The gravitational constant is represented by g. We consider the case where the channel is locally rectangular, so that

$$A = B(x) d(x, t), \qquad (2.5)$$

where B is the breadth and d the depth. The height is then h = h(x, t) = d(x, t) + z(x), where z is the height of the channel bed. Also K = A/M (hydraulic radius)^{2/3}, where Manning's constant M is taken as $0 \cdot 03$, and the hydraulic radius = A/wetted perimeter = A/(2A/B + B). This value of M and the form of K are found empirically and used widely for many problems.

3. FORMULATION

The schemes in [1] were developed for the idealized case where the breadth of the channel B = constant, the height of the bed z = constant, and no friction, so that the source term $\underline{s} = \underline{0}$. In order to extend, and then apply, these schemes to the general case given by equations (2.1)–(2.5), it is first necessary to rewrite these equations in the form,

$$\underline{W}_t + \underline{F}_x = \underline{S},\tag{3.1}$$

where

$$\underline{W} = (\phi, \phi u)^{\mathsf{T}} \tag{3.2}$$

$$\underline{F}(\underline{W}) = \left(\phi u, \phi u^2 + \frac{1}{2}\phi^2\right)^{-1}$$
(3.3)

$$\underline{S}(\underline{W}) = \left(-u\phi B'/B, -u^2\phi B'/B - g\phi z' - 0 \cdot 0009g\phi u |u| (\phi B/(2\phi + gB))^{-4/3}\right)^{4}$$
(3.4)

The independent variables are u = u(x, t), the fluid velocity, and

$$\phi = \phi\left(x,t\right) = gd\left(x,t\right) = g\left(h\left(x,t\right) - z\left(x\right)\right).$$

Note that the source term <u>S</u> on the right-hand side of (3.1) does not contain any derivatives of the flow variables ϕ and u and arises through variations in the channel and the friction terms. For future reference, the quasi-linear form of equation (3.1) is given by

$$\underline{W}_t + A \, \underline{W}_x = \underline{S},\tag{3.5}$$

where the Jacobian of the flux function \underline{F} is given by

$$A = \underline{F}_{\underline{W}} = \begin{pmatrix} 0 & 1\\ \phi - u^2 & 2u \end{pmatrix}.$$
 (3.6)

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