

# Characterization and phase transitions of $(\text{Bi,Pb})_2\text{Sr}_2\text{Ca}_2\text{Cu}_3\text{O}_x\text{-Ag}$ composite powder obtained by spray pyrolysis

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## Abstract

$(\text{Bi,Pb})_2\text{Sr}_2\text{Ca}_2\text{Cu}_3\text{O}_x\text{-Ag}$  (BPSCCO/Ag) composite precursor powder was prepared by spray pyrolysis. The as-prepared and thermally treated (750 °C (1 h) and 780 °C (3 h)) powders were characterized by transmission electron microscopy, ambient X-ray diffraction, In situ X-ray diffraction, magnetic susceptibility measurement and differential thermal analysis (DTA).

DTA curve exhibited two strong endothermic peaks above 790 °C, one very wide with the onset at 790 °C and the second at 840 °C. In situ X-ray diffraction measurements strongly supported the view that the first endothermic peak was due to  $\text{Ca}_2\text{PbO}_4$  decomposition and a transient liquid formation through  $\text{PbO-CuO-Ag}$  eutectic. The second endothermic peak can be explained by onset of Bi-2212 peritectic melting that began at 840 °C with local formation of Bi-2201 intergrowths. The melting was complete at 875 °C.

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## 1. Introduction

There are a few reports on metal/simple-oxide composite powders prepared by the spray pyrolysis route [1–3]. Majumdar et al. [2], for example, described the formation of Ag–CuO composite powder, while Matsumoto et al. [3] demonstrated viability of preparation of Ag–TiO<sub>2</sub> composite powder. Studies of metal/complex oxide composite powders, synthesized by spray pyrolysis, are even rarer. A study like this was performed by Tsudo et al. [4] on BPSCCO/Ag system. They studied the influences of the chemical composition of the precursor and the sintering conditions on the superconducting properties of (Bi,Pb)-2223 phase, such as  $T_c$  and  $J_c$ , and observed that the addition of Ag decreased both  $T_c$  and  $J_c$ .

Aerosol decomposition routes, such as spray pyrolysis, possess several advantages (chemical homogeneity of pow-

der, uniform-sized particles, etc.) over conventional solid-state techniques [5]. The quality of the powders obtained by spray pyrolysis can be further improved by the addition of urea to the metal nitrates precursor solution [6]. The preparation of a BPSCCO/Ag composite powder containing chemically homogeneous, uniform-sized submicron BPSCCO particles, mixed with well dispersed silver could be useful in fusion-reformation process for obtaining Bi-2212 and (Bi,Pb)-2223 bulks, tapes or films. This is due to the important role that silver plays in the reduction of oxygen losses upon peritectic melting [7] of these two superconducting phases. The minimization of oxygen losses on melting should help the reformation of Bi-2212 and (Bi,Pb)-2223 during the solidification process [7,8]. On the other hand, it has been reported [4,9] that the addition of high contents of silver can decrease the critical temperature of oxide superconductors. Since Jin et al. [10] showed that the addition of 20% of silver did not affect the critical temperature of BSCCO phases, this weight percent of silver was chosen in the present work.

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Presented here is a report on the characterization of BPSCCO/Ag composite powders as-synthesized by spray pyrolysis and after a rapid thermal treatment at 750 °C (1 h) and 780 °C (3 h). Afterwards, an in situ synchrotron X-ray diffraction study of the phase transitions that occur in the precursor powder was performed before the final conversion to (Bi,Pb)-2223 phase. The results of this study are supplemented by differential thermal analysis (DTA).

## 2. Experimental

Composite particles of Ag:(Bi,Pb)-2223 stoichiometry were synthesized from a mixed nitrate solution with the appropriate ratio of the cations necessary to produce the (Bi,Pb)-2223 phase (Bi:Pb:Sr:Ca:Cu = 1.8:0.2:2:2:3). The nominal concentration corresponds to 100 g of mixed metal oxides accomplished through dissolving of nitrates into 1000 ml of a 5 wt% HNO<sub>3</sub> water solution with 2 wt% urea and 20 wt% Ag (in the form of AgNO<sub>3</sub>). The precursor solution characteristics (density, pH, viscosity and surface tension) were measured and used to calculate [11] the average droplet size (2725 nm) and the aerosol droplet density (<10<sup>14</sup> droplets m<sup>-3</sup>). The solution was atomized using an ultrasonic atomizer with the working frequency of 1.7 × 10<sup>6</sup> Hz. Aerosol decomposition was carried out in a tubular flow reactor in argon gas at temperatures up to 840 °C. The aerosol flow rate was determined by the argon flow rate (1.7 × 10<sup>-6</sup> m<sup>3</sup> s<sup>-1</sup>) and the reactor geometry (quartz tube characteristics: inner diameter 3.6 × 10<sup>-2</sup> m, length 6 × 10<sup>-1</sup> m), therefore the residence time of a droplet/particle at the maximum reaction temperature was 5 s. The powder was analyzed in two states: as-prepared (collected at the end of the high temperature tubular flow reactor) and thermally treated in air at 750 °C (1 h) and 780 °C (3 h). The heat-treated powder can be used as the precursor powder for conversion to (Bi,Pb)-2223.

Particle structure was characterized by transmission electron microscopy (TEM) together with X-ray energy dispersive spectroscopy (EDS), using a JEOL 2010 operating at 200 kV. The TEM sample preparation procedure was ultramicrotomy. In this method, the powder is first embedded in a resin and then cut in an ultramicrotome (Reichert-Jung with a Diatome diamond knife), allowing the study of the particles internal structure.

Phase analysis of the as-prepared and heat-treated powders was completed using a Siemens D-5000 diffractometer. Cu K $\alpha$  radiation and graphite monochromator were used with a 0.02 scanning step and a step time of 25 s. Magnetic susceptibility measurements were performed by an AC susceptometer Lake Shore 7000 (using magnetic field of 1 Oe and frequency of 100 Hz) in the temperature range of 80–130 K.

DTA and in situ X-ray diffraction were used to study the reactions that precede the conversion of the composite precursor powder to Ag:(Bi,Pb)-2223. DTA of the heat-treated sample was carried out under static air atmosphere up to 900 °C

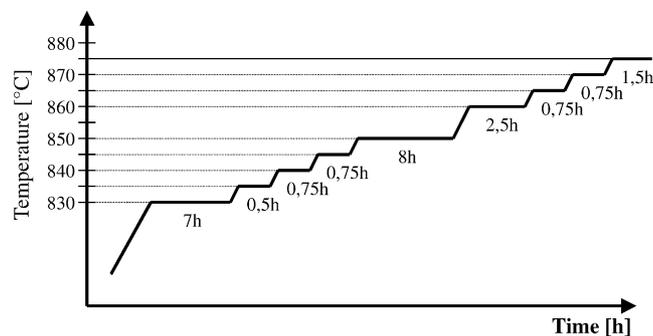


Fig. 1. Temperature–time schedule between 830 and 875 °C applied for in situ X-ray diffraction of the thermally treated powder.

in a Perkin-Elmer DTA-7. The heating rate was 10 °C min<sup>-1</sup>. In situ X-ray diffraction experiments of the thermally treated powder were carried out at the XRD1 beam-line station of the Brazilian National Synchrotron Light Laboratory (LNLS). The powder was heated from room temperature up to 740 °C at a rate of 20 °C min<sup>-1</sup>. From this temperature up to 830 °C, one pattern was taken every 5 °C. The exposure time for every pattern was about 10 min. From 830 °C a temperature–time schedule was applied up to the highest temperature measured of 875 °C, Fig. 1. One pattern was taken every 10 min in this temperature range. The step size was of 0.05° (2 $\theta$ ). The wavelength was 1.54068 Å ( $\Delta\lambda = 0.001617$ ), which was calibrated with silicon standard NBS640b.

Quantitative phase analysis of the room temperature patterns was carried out using the Rietveld method and the software Topas 2.1 [12].

## 3. Results and discussion

The X-ray diffraction patterns of the as-prepared and heat-treated powders (Fig. 2a and b) were analyzed quantitatively by the Rietveld method and the results are shown in Table 1. The as-prepared powder contains Bi-2212, Bi-2201, cuprate 14:24 (Sr<sub>14-x</sub>Ca<sub>x</sub>Cu<sub>24</sub>O<sub>41</sub>), CuO and Ag, while the heat-treated powder consists mainly of Bi-2212 and some secondary phases, such as cuprate 14:24, Ca<sub>2</sub>PbO<sub>4</sub> and Ag. The cuprate 1:1 (Ca<sub>1-x</sub>Sr<sub>x</sub>CuO<sub>2</sub>) is present in a very small content (less than 1%). The amount of silver in the as-prepared powder is overestimated due to the presence of amorphous material that was not taken into consideration in the full

Table 1

Relative weight percentages of the phases present in as-prepared and heat-treated powders

	As-prepared	Heat-treated
Bi-2212 (%)	31.8	62.1
Bi-2201 (%)	17.5	–
14:24 (%)	19.2	14.1
CP (%)	–	6.2
1:1 (%)	–	0.8
CuO (%)	7.8	–
Ag (%)	23.7	16.8

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